

NANCEE;
AN APPROACH TO BARRIER
SONOBUOY PATTERN OPTIMIZATION

Ralph Conrad Hilzer

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THESIS

NANCEE
AN APPROACH TO BARRIER
SONOBUOY PATTERN OPTIMIZATION

by

Ralph Conrad Hilzer, Jr.

June 1974

Thesis Advisor:

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NANCEE executes rapidly, and is easy to use and understand.

NANCEE
an Approach to Barrier
Sonobuoy Pattern Optimization

by

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Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN COMPUTER SCIENCE

from the

NAVAL POSTGRADUATE SCHOOL
June 1974

ABSTRACT

NANCEE is a computer simulation program which uses convolution (or meeting) probabilities to determine which barrier type of sonobuoy pattern has the highest probability of detection for a transiting nuclear submarine.

The program assumes that the optimum barrier is a straight-line one, two, or three row sonobuoy pattern containing not more than 48 sonobuoys. The barrier is centered on the submarine's expected line of transit, oriented perpendicular to the submarine's course, and placed far enough ahead of the submarine's position that all pattern sonobuoys are in the water and being monitored before the submarine enters the detection range of the sonobuoy pattern. If more than one barrier is found to have the highest probability of detection, the one with the least number of sonobuoys is selected as optimum.

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To Wally, Nancee, and Diane

My three favorite friends

I. INTRODUCTION

A. THE PROBLEM

Much of the guesswork was removed from aircraft sonobuoy pattern planning with the advent of readily available acoustic propagation-loss curves (see Figure 1). From them, the range at which a sonobuoy will detect a submarine can be estimated by predicting the path of the sound waves in water. Hence a logical estimate of the best sonobuoy pattern spacing is possible. However, two pattern planning questions remain unanswered. They are:

1. What should the shape of the pattern be? (i.e. circular, rectangular, diamond shaped, etc.)

2. How many sonobuoys should the pattern contain?

Some knowledge regarding characteristics of the target is desirable before the optimum sonobuoy pattern shape and number of sonobuoys can be determined. In general terms, the target may have either nuclear or diesel propulsion, and its current mode of operation may be:

1. Transiting (i.e. proceeding from home-port to an on-station position)

2. Holding (i.e. a fleet ballistic missile submarine operating on station)

or,

3. Tracking (i.e. intercepting and/or shadowing a high-value commercial or naval ship)

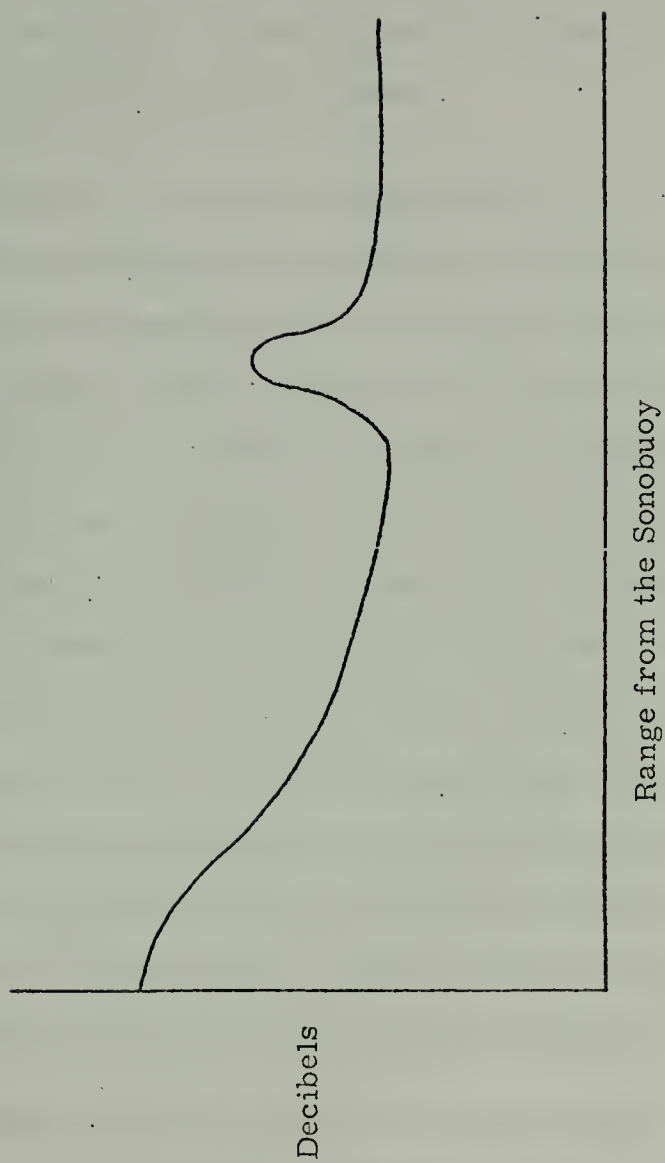


Figure 1
Propagation-Loss Curve Example

An algorithm which would single out the optimum pattern solution for each combination of the above target types and missions is preferred.

The object is to maximize the submarine probability-of-detection (POD) with minimum cost in material. Failure means that the target has been allowed to perform its mission undetected, and the expended pattern sonobuoys, aircraft flight time, flight crew time, and hours of ground preparation were wasted.

B. TENDENCY TO OVERCOMPENSATE

Because of the high cost of failure, there is a tendency to overcompensate and use an excessive number of sonobuoys in the pattern. This tendency would be appropriate if an aircraft could concurrently receive and process information from an unlimited number of sonobuoys, and if there were no limit to the radio-frequency range at which an aircraft could monitor pattern sonobuoys. However, only sixteen sonobuoy channels can be simultaneously monitored by an aircraft, and the sonobuoy monitor range is limited by atmospheric conditions and the curvature of the earth (see Appendix A). Because of the limited radio-frequency range and the aircraft's limited monitoring capacity, there is a maximum number of sonobuoys beyond which no increase of a pattern's POD is possible. No matter how tempting it may seem, exceeding this limit wastes expensive sonobuoys.

C. COMPUTER SIMULATION AS A SOLUTION

In order to determine the optimum pattern it will be necessary to make comparisons between a large number of potential solutions. Because of this, it is natural to turn to computer simulation as a means of solving the problem.

As a matter of fact, considerable effort has already been put forth to develop a computer program which optimizes sonobuoy patterns. Tactical Airborne Sonar Decision Aid (TASDA) [Ref. 2 and 3] is one such program. A good deal of realism has been incorporated into TASDA, and a variety of problem types are considered by it (including the holding and transiting of both nuclear and diesel submarines). Unfortunately, in the development of realism, the program became overly large both in terms of core requirements and program execution time. Repetitive POD computations and comparisons aggravates the execution time problem. Hence, for at least some problems it is necessary to reduce the execution time. A tempting technique is to reduce the number of submarine simulation runs through the sonobuoy pattern for each probability calculation. Unfortunately, this approach leads to a trade-off between a reasonable execution time and accurate probability estimates.

Another problem is that TASDA can consider not more than 20 sonobuoy pattern geometries, and each geometry is limited to 16 or fewer sonobuoys. This is only a small fraction of the patterns which current anti-submarine aircraft are capable of deploying. The addition of more pattern geometries to TASDA, or a program adaptation to handle more than 16 sonobuoys per geometry would even further aggravate the execution time problem.

Based on the above considerations, an alternative approach to the sonobuoy pattern optimization problem was investigated.

II. ASSUMPTIONS

Assumptions made in order to limit the problem to realistically solvable terms are:

A. TARGET TYPE

The program should be oriented toward a continuously detectable noise source (i.e. a nuclear submarine) and transiting between two widely separated positions. Although narrowing the problem essentially to transiting nuclear submarines appears to be a severe limitation, bear in mind that long range capabilities make them a primary threat, and in order to reach most positions of operational interest, long transits are necessary.

B. SONOBUOY PATTERN SHAPE AND POSITION

The optimum tactic to be used against transiting nuclear submarines is a straight-line one, two, or three row sonobuoy pattern centered on the submarine's expected line of transit, placed ahead of its current position, and oriented perpendicular to the expected course. However, this is not intended to discourage consideration of "V" shaped (chevron) patterns. A chevron pattern is a simple variation of the straight-line case with a bend at pattern center. Certainly, the bending alters the pattern's POD, but if the bending angle is not large, the detection capability of the chevron pattern can be estimated from the POD of the equivalent straight-line pattern.

C. SONOBUOY SPACING

Sonobuoy spacing should be either determined inside the program or input to the program. The problem is restricted to the determination of the minimum number of sonobuoys which produce the maximum POD, with fixed sonobuoy spacing.

D. SONOBUOY LIMIT

The optimum pattern should contain no more than 48 total sonobuoys. The difficulty in monitoring and maintaining patterns of larger size has a disruptive effect which outweighs any increase in POD.

E. PROGRAM REALISM

Realism must sometimes be sacrificed. For instance, random equipment failures, sonobuoy failures, and monitor sequence disruption (due to prosecution of false contacts, improper adherence to monitor cycle instructions, etc.) are considered too costly to program, and therefore are not included in the program.

III. THE METHOD

A. PROGRAM NAME

With the assumptions of Chapter II as a start, a computer simulation program, hereafter referred to as NANCEE, was developed. NANCEE consists of a main program and seven subroutines:

RANGE

GEOM

TOSS

MEET

BUILD

MAKEUP

OUTPUT

Throughout the following discussion, program variables and arrays appear in capital letters, with their definitions contained in Appendix F.

B. APPROACH TO PROBABILITY CALCULATIONS

A sonobuoy pattern is divided into zones (see Figure 2) and probabilities deemed appropriate for each zone are summed to form an estimate of the pattern's overall POD.

First, the probability that a submarine will pass through each zone of a pattern is estimated (probability 1). Then, for each zone, the probability that a submarine passing through will be detected is estimated (probability 2). The product of these two zone probabilities ((probability 1)x(probability 2)) is the probability a submarine will pass through that zone and be detected. The sum of (probability 1)x (probability 2) for all zones is the sonobuoy pattern POD.

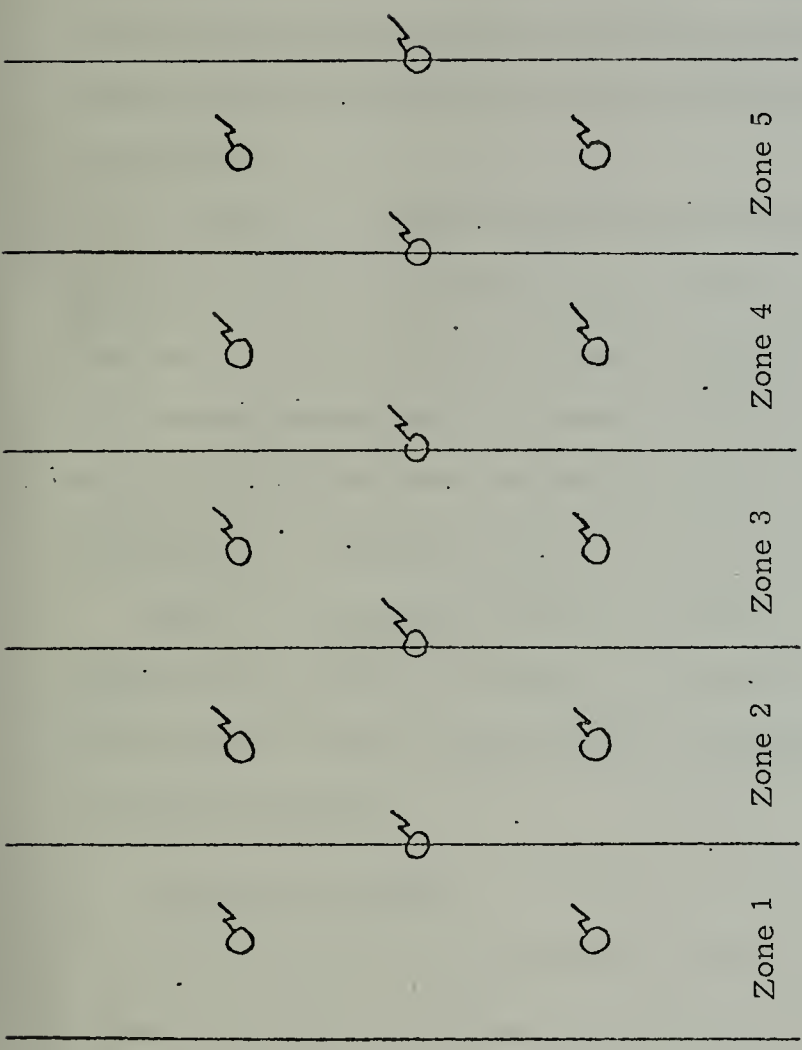


Figure 2
Division of Three-Row Sonobuoy Pattern into Zones

Probability 1 is estimated by using known or estimated submarine characteristics to generate random submarine tracks, and observing where these random tracks penetrate the pattern area.

Convolutional (or meeting) probabilities are used to estimate probability 2. For 10 sizes of predicted detection ranges, the probability that monitor time on at least one zone sonobuoy will overlap the time during which a submarine is within detection range of that sonobuoy is calculated. The average of these 10 calculations is probability 2.

In contrast, TASDA varies the sonobuoy spacing of several sonobuoy pattern geometries (one geometry at a time) from small to large spacings. Submarine simulations through the pattern area are used to generate submarine detections, and these detections are used to estimate POD's for each sonobuoy spacing. The geometry and sonobuoy spacing with the highest POD is selected as optimum.

Another computer simulation program, Search Tactics Evaluation Model (STEM) [Ref. 1] selects as optimum the pattern with the least number of gap areas inside which it is possible for the submarine to operate undetected.

C. THE SUBMARINE

The submarine is assumed to be making a straight-line transit on a course uniformly distributed between the limits of course accuracy (CUSACC), and with a mean of the expected submarine course (SUBCUS) in degrees true. The submarine's speed (SUBSPD) in knots remains constant throughout the transit.

D. INITIAL SUBMARINE PROBABILITY AREA

The initial submarine probability area is where the submarine is suspected to have been, at some fixed time in the past. It is datum. Realistically, the area may have any shape and size (i. e. diamond, eircular, elliptical, rectangular, etc.), but for the purposes of this program it is assumed to be rcctangular with no side longer than 1,000 nautical miles. The rectangle may be given any orientation, and the submarine position is assumed to bc uniformly distributed inside.

E. SONOBUOY PATTERN AREA

The center of each potential sonobuoy pattern evaluated by NANCEE is at a single precomputed position. This position is on the submarine's expected line of transit far enough ahead of the submarine's position that all sonobuoys are in the water and being monitored before the submarine cnters the pattern area. The sonobuoy patterns are all oriented perpendicular to the submarine's expected course and have a radius no larger than the extended radio-frequency range (see Appendix B). The GEOM subroutine prepares the initial submarine probability area and sonobuoy pattern area for simulation in the TOSS subroutine.

F. GENERATION OF 10 EQUALLY LIKELY DETECTION RANGES

On the avcrage, the rangc at which a submarine will be detected from a sonobuoy is the mean-detection range (or the least range at which the target figure-of-merit intersects the propagation-loss curve). But it is seldom that the first detection occurs exaetly at the mean-detection range. Somctimes the target is detected closer to the sonobuoy, sometimes further away. Recognizing this, the theory behind subroutine RANGE is that the propagation-loss curve varies

in accordance with a normal distribution with a standard deviation of SIGMA decibels. In turn, this randomly varying propagation-loss curve is used to generate RUNNR random detection ranges (see Appendix C).

From the RUNNR random detection ranges, ten are selected as equally likely representatives of the other random detection ranges. The random detection ranges are arranged in order from the smallest to the largest and then are counted in order starting with the smallest. The $(0.1 \times \text{RUNNR})$ th random detection range becomes the value of RANGES (I), where I varies from one to ten. It is intended that each element of the RANGES vector be close to the same length as one-tenth of the RUNNR random detection ranges, and therefore representative of them.

G. DISTRIBUTION OF SUBMARINE SIMULATION RUNS IN THE SONOBUOY PATTERN AREA

The size and shape of the initial submarine probability area along with time-late (TLATE) and the submarine's course accuracy (CUSACC) determine how submarine simulation runs originating from the initial submarine probability area are distributed in the potential sonobuoy pattern area. Knowledge of this distribution is essential in order to prudently evaluate potential sonobuoy positions.

To determine the distribution, the longest one-row sonobuoy pattern which has a spacing of BUOYSP nautical miles and still has a pattern radius less than ERFRNG nautical miles is centered in the sonobuoy pattern area. Each sonobuoy in this pattern is assumed to be continuously monitored with a detection range equal to the average detection range, RANGES (INDEX). NRTOSS submarine simulation

runs are sent through the sonobuoy pattern area. If the submarine is detected by a sonobuoy, that run is counted as a passage through a zone at that position in the pattern. There are NRBUOY sonobuoys in the pattern so there are NRBUOY zones through which passages can be detected. After the NRTOSS simulation runs, the number of passages through zone I (detections by sonobuoy number I) divided by NRTOSS equals DETECT (I), or the probability that a submarine will pass through zone I in the pattern. The TOSS subroutine generates this DETECT vector array.

Simulation runs which fail to pass through any sonobuoy pattern zone are assumed to be outside the detection range of the pattern and, thus, are impossible to detect. The number of those submarine simulation runs that do pass through the sonobuoy pattern area

$$\text{(i. e. } \sum_{I=1}^{\text{NRBUOY}} \text{DETECT (I)) divided by NRTOSS is the probability a submarine}$$
will pass through the largest potential sonobuoy pattern area, and is an upper limit for the probability a submarine will be detected while passing through any possible pattern centered in the sonobuoy pattern area.

H. DETECTION WITHIN A ZONE

Not every submarine passing through a sonobuoy pattern zone will be detected. For instance, if the detection ranges fail to overlap, it is possible for the submarine to pass undetected between the buoys. Also, a submarine may pass through the detection range of a sonobuoy at a time when it is unmonitored.

In calculating the zone POD's, it is assumed that the submarine is on its expected course (SUBCUS), or a course perpendicular to the orientation of the sonobuoy pattern. As the submarine passes through a sonobuoy pattern zone, it will cross one of three sub-areas within that zone defined as follows:

Segment 1 - An area where the portion of the sonobuoy detection range which the submarine must transit is longer than the distance the submarine travels during the unmonitored portion of a monitor sequence (see Figure 3). Theoretically, the probability of detecting a submarine crossing through a segment 1 area is 1.0 (note: DIST1 is a segment 1 area in Figure 6).

Segment 2 - An area where the portion of the sonobuoy detection range which the submarine must transit is long enough to produce a minimum recognizable write-out, but less than the distance the submarine travels during the unmonitored portion of a monitor sequence (see Figure 3). The submarine may or may not be detected while passing through a segment 2 area depending on the success of the monitor sequence. Computation of these probabilities, p_Z , called meeting probabilities is described in Appendix D (note: DIST2 - DIST1 is a segment 2 area in Figure 6).

Segment 3 - An area where the portion of the sonobuoy detection range which the submarine must cross through is less than the distance the submarine travels in six minutes (see Figure 3). Theoretically, the submarine will fail to produce a recognizable write-out, so the probability of detecting a submarine crossing a segment 3 area is 0.0.

Variation of the number of rows and the sonobuoy detection range in a zone alters the distribution of segment 1, segment 2, and segment 3

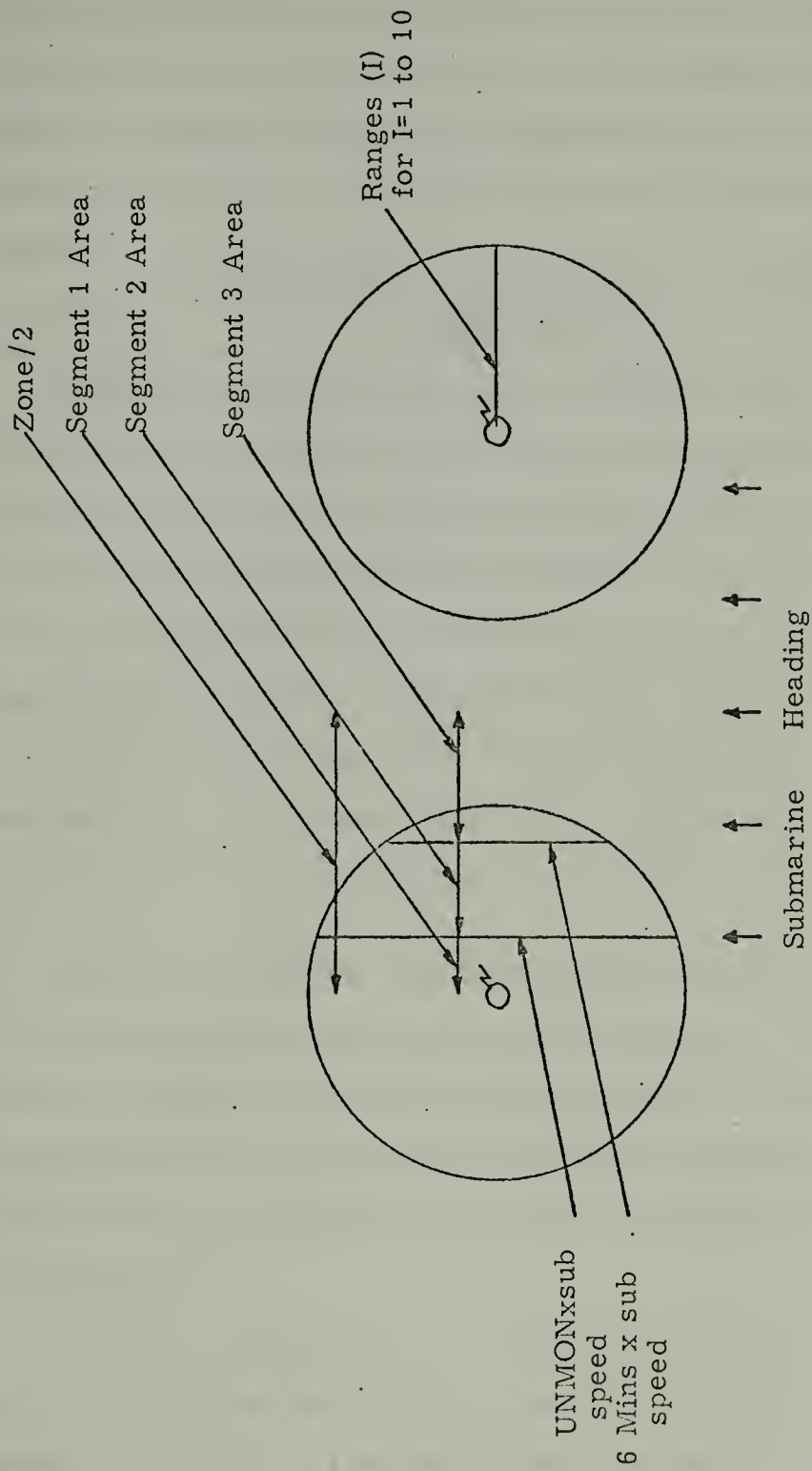


Figure 3

Segment 1, 2, and 3 Areas

areas within that zone. Similarly, variation of the monitor time and sequences per cycle alters the distribution because it changes the time sonobuoys are left unmonitored. If the sonobuoy detection range, number of sonobuoy pattern rows, and monitor plan are fixed for all sonobuoys in a zone, the POD for a submarine passing through that zone is,

$$\text{PROB} = \frac{1.0 \times (\text{segment 1}) + p_Z \times (\text{segment 2}) + 0.0 \times (\text{segment 3})}{(\text{zone length}) / 2}$$

PROB represents only one size of detection range. Recall, however, that earlier the generation of 10 equally likely detection ranges was discussed. Keeping the number of rows and the monitor plan fixed in a zone and computing PROB for each sized detection range, the sum divided by 10 is PD(I,J), or the probability an I row zone with each sonobuoy monitored using a J sequence monitor plan will detect the submarine (note: J equals one implies continuous monitoring). The purpose of the MEET subroutine is to generate the PD vector array for all combinations of I and J between one and three.

I. MONITOR SCHEMES FOR SONOBUOY PATTERNS

The monitoring aircraft is assumed to have a 16 channel monitor capacity. Consider an I row sonobuoy pattern. Which PD array element is appropriate in a zone of that pattern depends on how sonobuoys in that zone are monitored, or on which of the following four cases is appropriate:

Case 1 - There are 16 or fewer total sonobuoys in the pattern and the sonobuoy pattern radius is less than the radio-frequency range. Sonobuoys in all zones are considered to be continuously monitored, so POD in each zone is PD(I, 1).

Case 2 - There are between 17 and 32 total sonobuoys in the pattern and the sonobuoy pattern radius is less than the radio-frequency range. It is necessary to monitor sonobuoys in the pattern in two sequences. The zones extending inward from one side of the pattern containing a total of 16 sonobuoys comprise one sequence. Similarly, the zones extending inward from the other side of the pattern containing a total of 16 sonobuoys comprise the other sequence. With this arrangement, it is possible for zones toward the center of the sonobuoy pattern to belong to both sequences. Sonobuoys in these zones are considered to be continuously monitored, so POD in these zones is $PD(I, 1)$. Sonobuoys in all other zones are affected by the two-sequence monitor plan and are considered to be monitored for BMON hours and then left unmonitored for UNMON(2) hours during each monitor cycle. POD in these zones is $PD(I, 2)$.

Case 3 - There are more than 32 sonobuoys in the pattern and the sonobuoy pattern radius is less than the radio-frequency range. It is necessary to monitor sonobuoys in the pattern in three sequences. Two of the sequences are the same as was defined in case 2. The zones centered at pattern center and which contain a total of 16 sonobuoys comprise the third sequence. Sonobuoys in zones which belong to all three sequences are considered to be continuously monitored, so POD in these zones is $PD(I, 1)$. Sonobuoys in zones which belong to two of the three sequences are considered to be monitored in accordance with the two sequence scheme of case 2, so POD in these zones is $PD(I, 2)$. Finally, sonobuoys in zones which belong to only one sequence are considered to be monitored for BMON hours and left unmonitored for UNMON(3) hours during each monitor cycle, so POD in these zones is $PD(I, 3)$.

Case 4 - The sonobuoy pattern radius is greater than the radio-frequency range. It is necessary to monitor sonobuoys in the pattern in three sequences (see Appendix B). The only difference between case 4 and case 3 is that in case 4, the number of sonobuoys per sequence is the total which fit inside the radio-frequency range, but which do not exceed a total of 16.

J. SONOBUOY PATTERN PROBABILITIES

The PD and DETECT vector arrays are the ingredients used to construct sonobuoy pattern probabilities in the BUILD subroutine.

DETECT(K) is the probability that a submarine will pass through zone K in the potential sonobuoy pattern area (where K is between 1 and NRBUOY). In comparison, PD(I, J) is the probability that if a submarine passes through any zone, an I row zone monitored using J sequences will detect the submarine. Hence,

$$p_K = PD(I, J) \times DETECT(K)$$

is the probability that the submarine will pass through zone K and be detected.

Construction of a sonobuoy pattern POD consists of:

1. Fixing the number of rows, I, in the pattern (between one and three).
2. Determining which zones the pattern will cover (centered in the potential sonobuoy pattern area). For example, N zones extending from zone z_1 to z_N .
3. Individually determining how each of the N zones in the sonobuoy pattern are to be monitored (which of the four cases in the previous section is appropriate for the pattern).

4. Summing p_K for each zone in the pattern, or

$$PVEC(I, N) = \sum_{K=z_1}^{z_N} p_K.$$

$PVEC(I, N)$ is the POD of an I row pattern consisting of N zones.

The total number of sonobuoys in this sonobuoy pattern is $I \times N$.

K. SELECTION OF THE OPTIMUM PATTERN

The program builds POD's for all possible one, two, and three row sonobuoy patterns which have: A sonobuoy spacing equal to BUOYSP nautical miles, contain 48 or fewer sonobuoys, and which have a radius less than the extended radio-frequency range. The pattern with the highest POD (largest PVEC value) is selected as the optimum pattern. If more than one pattern has the highest POD, the one with the least total number of sonobuoys is selected as optimum.

IV. PROGRAM INPUTS AND OUTPUTS

A. INPUTS

The main program reads in values for program variables and arrays which require initialization. The read-in values are then tested to ensure they are within certain prescribed limits, and if not, the program is terminated. For a further description of program inputs see Appendix E.

B. NANCEE MAKEUP

Subroutine MAKEUP prints out the RANGES, DETECT, and PD vector arrays used to construct the sonobuoy pattern probabilities. This makes possible an in-depth analysis of the POD calculations. See Table I for an example of NANCEE MAKEUP.

C. NANCEE OUTPUT

Subroutine OUTPUT prints out:

1. All sonobuoy pattern descriptions and POD's which were considered in the selection of the optimum pattern. This section permits consideration of sonobuoy patterns which have POD's close to the POD of the optimum pattern, but which have fewer total sonobuoys.
2. Important program inputs (note: the propagation-loss heading information is a copy of the first two cards of Fleet Numerical Weather Central Monterey's propagation-loss curve data deck).
3. A description of the optimum pattern along with the optimum POD.

NANCEE MAKEUP

RANGES ARRAY

11.9
11.9
20.7
20.7
20.7
21.7
22.2
22.2
22.1

DETECT ARRAY

0.02000 0.04200 0.05800 0.04400 0.05200 0.04200 0.06600 0.03600 0.04600 0.04000

PC ARRAY FCMS SEQUENCES

0.5629 1
0.9550 1
0.9124 1
1.0000 2
1.0000 2
0.9772 3
1.0000 3
0.5966 3

TABLE I
An Example of NANCEE MAKEUP

and,

4. Optimum pattern orientation, spacing, location, and monitoring parameters.

See Table II for an example of NANCEE OUTPUT.

NANCEE OUTPUT

ROWS SONOBUDYS	PD	ROWS SONOBUDYS	PD	ROWS SONOBUDYS	PD
1	0.0404	2	0.0420	3	0.0420
1	0.1040	4	0.1020	9	0.1080
1	0.1541	6	0.1600	9	0.1600
1	0.1947	8	0.1900	13	0.1900
1	0.2351	10	0.2400	13	0.2400
1	0.2757	12	0.2869	13	0.2800
1	0.3172	14	0.3440	22	0.3440
1	0.3597	16	0.3840	24	0.3840
1	0.4020	18	0.4300	27	0.4300
1	0.4445	20	0.4720	30	0.4720
1	0.4872	22	0.4974	33	0.4965

PPGREAM INPUTS

PROFLOSS CURVE
 HEADING INFORMATION: IMR26
 FIGURE CF-ME: 95.6 DB
 SUBMARINE SPEED: 20 KNOTS
 SUBMARINE COURSE: 25 DEGREES TRUE
 SUBMARINE COURSE: 50 DEGREES
 INITIAL SUBMARINE PROBABILITY AREA: X1= 10.0 X2= 10.0 X3= -10.0 X4= -10.0
 Y1= -50.0 Y2= 50.0 Y3= 50.0 Y4= -50.0
 TIME LATE: 12.5 HOURS
 AIRCRAFT ON-STATION SPEED: 180 KNOTS
 AIRCRAFT ON-STATION ALTITUDE: 20000 FEET

OPTIMUM PATTERN: 2 ROWS 22 SONOBUDYS - PROBABILITY-CF-DETECTION= 0.4974

1*	2*	3*	4*	5*	6*	7*	8*	9*	10*	11*
12*	13*	14*	15*	16*	17*	18*	19*	20*	21*	22*

OPTIMUM PATTERN PARAMETERS

ORIENTATION: 115/295 DEGREES TRUE
 SONOBUDY SPACING: 29 NAUTICAL MILES
 RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CENTER TO SONOBUDY PATTERN CENTER: 376.7 NAUTICAL MILES/ 25 DEGREES TRUE
 USE 3 3/4 MINUTE MONITOR CYCLES

TABLE II
 An Example of NANCEE OUTPUT

V. APPLICATIONS AND EXAMPLES

A. PROGRAM EXECUTION TIME

In the planning stages, it was hoped that NANCEE would execute in less than two minutes when the program reached its final form. In fact, the operating program substantially improves on this expectation. The average execution time with various input combinations has been 20 to 30 seconds. The most time consuming problems were those with small sonobuoy spacings (mini-barriers) because they generate a large number of sonobuoy pattern zones. For instance, one mini-barrier problem generated 43 zones and required 1 minute 9.88 seconds of execution time. Based on this testing, low execution time appears to be one of NANCEE's positive features.

B. NORMAL OPTIMUM PATTERN SELECTIONS

NANCEE normally selects a one or two-row sonobuoy pattern as optimum. The few times that a three-row pattern was selected, the increase in POD over the best two-row pattern was not significant.

C. THE MODE 2 PROGRAM FUNCTION

If MODE equals 1 (see Appendix E), the sonobuoy spacing (BUOYSP) is set internally to $1.41421 \times \text{RANGES}(\text{INDEX})$. However, this spacing is not guaranteed to be the one that produces the maximum sonobuoy pattern POD. It is no more than a good logical estimate. By setting MODE to 2, it is possible to input sonobuoy spacing as well as sonobuoy monitor time per cycle by data card.

To illustrate the use of MODE 2, Tables III and IV are NANCEE MAKEUP and NANCEE OUTPUT for a problem executed in MODE 1. An exceptional POD of 0.9544 for a 3 row 21 sonobuoy pattern with a sonobuoy spacing of 48 nautical miles was found to be optimum. Some small detection ranges in the RANGES vector array of NANCEE MAKEUP indicated that a smaller sonobuoy spacing was worthy of consideration. Hence, a 20 nautical mile sonobuoy spacing was input using MODE 2. Tables V and VI are NANCEE MAKEUP and NANCEE OUTPUT for this MODE 2 case. The optimum pattern this time was a single row 13 sonobuoy pattern, which is nine sonobuoys less than the MODE 1 case. Notice, however, that the POD, although still an exceptional 0.938, is somewhat less than the MODE 1 POD.

D. PROPACATION -LOSS CURVE SHORTENING

Best results are obtained when the detection ranges generated in the RANGE subroutine are direct path ranges. Convergence zone ranges tend to inflate both the optimum pattern's POD and MODE 1 sonobuoy spacing. Usually convergence zones are found at distances greater than 30 nautical miles from a sonobuoy, so it is possible to chop off the portion of the propagation-loss curve past the first convergence zone (by reducing NPLPTS) thus forcing the program to only work with direct path ranges. Tables VII and VIII are NANCEE MAKEUP and NANCEE OUTPUT in a case where all 250 kiloyards of a propagation-loss curve with strong convergence zones was used (NPLPTS equals 250). The optimum sonobuoy pattern is a 2 row 12 sonobuoy pattern with a sonobuoy spacing of 57 nautical miles and a POD of 0.9582. Tables IX and X are NANCEE MAKEUP and NANCEE

RANGES ARRAY

12.3
18.3
21.7
27.7
34.1
40.5
47.9
57.3
71.1
115.6

DETECT ARRAY

0.0500 0.17200 0.19000 0.20800 0.16800 0.10800 0.07200

PC ARRAY ROWS SEQUENCES

0.9177	1	1	1	2	3	1	2	3
0.8997	1	1	1	2	3	1	2	3
0.8306	1	1	1	2	3	1	2	3
1.0000	1	1	1	2	3	1	2	3
0.5758	1	1	1	2	3	1	2	3
0.8955	1	1	1	2	3	1	2	3
1.0000	1	1	1	2	3	1	2	3
0.5846	1	1	1	2	3	1	2	3
0.9236	1	1	1	2	3	1	2	3

TABLE III

NANCEE MAKEUP for MODE 1 Part of MODE 1 / MODE 2 Comparison

NANCEE OUTPUT

ROWS SONBUOYS	PD	ROWS SONBUOYS	PD	ROWS SONBUOYS	PD
1	0.1901	2	0.2080	3	0.2080
1	0.3451	2	0.3760	3	0.3760
1	0.5194	2	0.5660	3	0.5660
1	0.6165	2	0.6740	3	0.6740
1	0.7104	2	0.8460	3	0.8460
1	0.8425	2	0.9180	3	0.9180
1	0.9372	2	0.9501	3	0.9544

PROGRAM INPUTS

PROPLOSS CURVE
HEADING INFORMATION: 19022
FIGURE-CF-MERIT: 75.2 DM
SUBMARINE SPEED: 20 KNOTS
SUBMARINE COURSE: 124 DEGREES TRUE
SUBMARINE COURSE ACCURACY: 43 DEGREES
INITIAL SUBMARINE PROBABILITY AREA: X1= 5.0 X2= 45.0 X3= -5.0 X4= -45.0
Y1= 105.0 Y2= 95.0 Y3= -105.0 Y4= -95.0
TIME LATE: 6.4 HOURS
AIRCRAFT ON-STATION SPEED: 200 KNOTS
AIRCRAFT ON-STATION ALTITUDE: 10000 FEET

OPTIMUM PATTERN: 3 ROWS 21 SONBUOYS - PROBABILITY-OF-DETECTION= 0.9544

1°	2°	3°	4°	5°	6°	7°
8°	9°	10°	11°	12°	13°	14°
15°	16°	17°	18°	19°	20°	21°

OPTIMUM PATTERN PARAMETERS

ORIENTATION: 34/214 DEGREES TRUE
SONBUOY SPACING: 4 NAUTICAL MILES
RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CENTER TO SONBUOY PATTERN CENTER: 286.8 NAUTICAL MILES/124 DEGREES TRUE
USE 3 61 MINUTE MCNITER CYCLES

TABLE IV

NANCEE OUTPUT for MODE 1 Part of MODE 1/MODE 2 Comparison

NANCEE MAKEUP

RANGES ARRAY

12:3
18:3
21:7
27:7
34:1
40:5
47:9
57:3
71:1
115:6

DETECT ARRAY

0.04400	0.08000	0.02800	0.06400	0.07400	0.11200	0.08200	0.08800	0.06000	0.09600
0.05600	0.03600	0.05800							

PC ARRAY ROWS SEQUENCES

1.0000	1	1
1.0000	1	1
1.0000	1	1
1.0000	2	1
1.0000	2	1
1.0000	2	1
1.0000	3	1
1.0000	3	1
1.0000	3	1

TABLE V

NANCEE MAKEUP for MODE 2 Part of MODE 1/MODE 2 Comparison

NANCEE OUTPUT

ROWS SONBUOYS	PO	ROWS SONBUOYS	PO
1	0.0820	1	0.0820
2	0.1700	2	0.1700
3	0.2820	3	0.2820
4	0.3420	4	0.3420
5	0.4160	5	0.4160
6	0.5120	6	0.5120
7	0.5720	7	0.5720
8	0.6320	8	0.6320
9	0.7200	9	0.7200
10	0.7560	10	0.7560
11	0.8360	11	0.8360
12	0.8940	12	0.8940
13	0.9380	13	0.9380

PROGRAM INPUTS

FIGURE OF MERIT: 1201 FT. FREQ .300 KHZ SEA STATE 2 60 FT. RCVR AT 60 FT. 74020000
 HEADING INFORMATION: 18022
 FIGURE OF MERIT: 75.200
 SUBMARINE SPEED: 20 KNOTS
 SUBMARINE COURSE: 124 DEGREES TRUE
 SUBMARINE COURSE: 123 DEGREES
 INITIAL SUBMARINE PROBABILITY AREA: X1= 5.0 X2= 45.0 X3= -9.0 X4= -45.0
 Y1= 105.0 Y2= 95.0 Y3= -105.0 Y4= -95.0
 TIME LATE: 6.4 HOURS
 AIRCRAFT ON-STATION SPEED: 200 KNOTS
 AIRCRAFT ON-STATION ALTITUDE: 10000 FEET

OPTIMUM PATTERN: 1 ROWS 13 SONBUOYS - PROBABILITY-OF-DETECTION= 0.9380

1* 2* 3* 4* 5* 6* 7* 8* 9* 10* 11* 12* 13*

OPTIMUM PATTERN PARAMETERS

ORIENTATION: 34/214 DEGREES TRUE
 SONBUOY SPACING: 20 NAUTICAL MILES
 RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CENTER TO SONBUOY PATTERN CENTER: 266.8 NAUTICAL MILES/124 DEGREES TRUE
 MONITOR ALL PATTERN SONBUOYS CONTINUOUSLY

TABLE VI

NANCEE OUTPUT for MODE 2 Part of MODE 1/MODE 2 Comparison

RANGES ARRAY

12.8
20.2
39.5
40.0
41.0
41.5
42.5
77.0
80.5
119.5

DETECT ARRAY

0.06400 0.21000 0.24000 0.20800 0.16800 0.07800

PC ARRAY ROWS SEQUENCES

0.9159	1	1
0.9052	1	2
0.8681	1	3
0.9858	2	1
0.9760	2	2
0.9278	2	3
0.9858	3	1
0.9801	3	2
0.9462	3	3

TABLE VII

NANCEE MAKEUP for Propagation-Loss Curve Shortening Example - NPLPTS = 250

ROWS SONBUOYS
1 1 1 1 1 1
2 3 4 5 6
PO
0.2190
0.4103
0.6026
0.7565
0.8151
0.8860

ROWS SONBUOYS
2 2 2 2 2 2
PO
0.2376
0.4434
0.6513
0.8176
0.8809
0.9582

ROWS SONBUOYS
3 3 3 3 3 3
PO
0.2376
0.4434
0.6513
0.8176
0.8809
0.9568

PROGRAM INPUTS

PROCPLOSS CURVE
HEADING INFORMATION: 1A103 DEPTH 14400 FT. FREQ .300 KHZ SEA STATE 2 60 FT. RCVR AT 90 FT 94020000
FIGURE-OF-MERIT: 88.2 DB
SUBMARINE SPEED: 20 KNOTS
SUBMARINE COURSE: 124 DEGREES TRUE
SUBMARINE COURSE ACCURACY: 23 DEGREES EITHER SIDE OF COURSE
INITIAL SUBMARINE PROBABILITY AREA: X1= 105.0 X2= 45.0 X3= -5.0 X4= -45.0
TIME LATE: 6-4 HOURS
AIRCRAFT ON-STATION SPEED: 180 KNOTS
AIRCRAFT ON-STATION ALTITUDE: 20000 FEET

OPTIMUM PATTERN: 2 ROWS 12 SONBUOYS - PROBABILITY-OF-DETECTION= 0.9582

1* 2* 3* 4* 5* 6*
7* 8* 9* 10* 11* 12*

OPTIMUM PATTERN PARAMETERS

ORIENTATION: 34/214 DEGREES TRUE
SONBUOY SPACING: 57 NAUTICAL MILES
RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CENTER TO SONBUOY PATTERN CENTER: 303.0 NAUTICAL MILES/124 DEGREES TRUE
MONITOR ALL PATTERN SONBUOYS CONTINUOUSLY

TABLE VIII

NANCEE OUTPUT for Propagation-Loss Curve Shortening Example - NPLPTS = 250

NANCEE MAKEUP

RANGES ARRAY

9.4
10.4
11.4
12.5
13.6
14.8
15.8
18.7
20.7
29.1

DETECT ARRAY

0.02400 0.05600 0.07000 0.07400 0.05000 0.08000 0.08800 0.09600 0.06600 0.05400
0.06600 0.06200 0.06000 0.02400 0.03400

40

PC ARRAY ROWS SEQUENCES

0.5982 1
0.5960 1
0.5837 1
1.0000 2
1.0000 2
1.0000 2
1.0000 3
1.0000 3
1.0000 3

TABLE IX

NANCEE MAKEUP for Propagation-Loss Curve Shortening Example - NPLPTS = 71

ROWS SONBUOYS	PO	ROWS SONBUOYS	PO
1	0.0960	3	0.0960
2	0.1620	4	0.1620
3	0.2500	5	0.2500
4	0.3040	6	0.3040
5	0.3840	7	0.3840
6	0.4500	8	0.4500
7	0.5060	9	0.5060
8	0.5680	10	0.5680
9	0.6420	11	0.6420
10	0.7020	12	0.7020
11	0.7720	13	0.7720
12	0.8520	14	0.8520
13	0.8860	15	0.8860
14	0.9100	16	0.9100

PROGRAM INPUTS

PROPLUSS CURVE
 HEADING INFORMATION: 14103 DEPTH 14400 FT. FREQ .300 KHZ SEA STATE 2 60 FT. RCVR AT 40 FT. 74020000
 FIGURE-OF-MERIT: 85.2 DB
 SUBMARINE SPEED: 20 KNOTS
 SUBMARINE COURSE: 124 DEGREES TRUE
 SUBMARINE COURSE ACCURACY: 33 DEGREES EITHER SIDE OF COURSE
 INITIAL SUBMARINE PROBABILITY AREA: X1= 105.0 X2= 45.0 X3= -5.0 X4= -45.0
 TIME LATE: 6.4 HOURS
 AIRCRAFT ON-STATION SPEED: 180 KNOTS
 AIRCRAFT ON-STATION ALTITUDE: 20000 FEET

OPTIMUM PATTERN: 2 ROWS 30 SONBUOYS - PROBABILITY-OF-DETECTION= 0.9100

1*	2*	3*	4*	5*	6*	7*	8*	9*	10*	11*	12*	13*	14*	15*
16*	17*	18*	19*	20*	21*	22*	23*	24*	25*	26*	27*	28*	29*	30*

OPTIMUM PATTERN PARAMETERS

ORIENTATION: 34/214 DEGREES TRUE
 SONBUOY SPACING: 19 NAUTICAL MILES
 RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CENTER TO SONBUOY PATTERN CENTER: 282.2 NAUTICAL MILES/124 DEGREES TRUE
 USE 3 15 MINUTE MONITOR CYCLES

TABLE X

NANCEE OUTPUT for Propagation-Loss Curve Shortening Example - NPLPTS = 71

OUTPUT for a problem with identical inputs except NPLPTS has been reduced to 71 to exclude all convergence zones. The optimum sonobuoy pattern this time is a 2 row 30 sonobuoy pattern with an 18 nautical mile sonobuoy spacing and a POD reduced somewhat to 0.91. The pattern computed without convergence zones will produce more reliable results.

E. PROPAGATION-LOSS CURVES WITH ZIG-ZAG PATTERNS

For the same reason that propagation-loss curves with strong convergence zones can cause problems, propagation-loss curves with zig-zag patterns (curves which alternate radically between high and low decibel levels) can also be a problem. An extreme example of this was input to test the program. NANCEE MAKEUP and NANCEE OUTPUT in Tables XI and XII appear to be quite reasonable solutions to the problem. Randomization of IRANGE (see Appendix C) deserves credit for this success.

F. A COMPARISON WITH TASDA AC

NANCEE and TASDA AC [Ref. 2] were programmed with identical inputs to form a comparison between the two programs. NANCEE MAKEUP and NANCEE OUTPUT for the comparison are in Tables XIII and XIV.

NANCEE selected a 2 row 12 sonobuoy pattern with a sonobuoy spacing of 30 nautical miles as optimum. TASDA AC, programmed to consider 10 geometries and using 20 submarine simulation runs per probability calculation, selected a box-shaped pattern with 16 sonobuoys and a 57 nautical mile spacing.

RANGES ARRAY

6.9
13.8
13.3
14.7
27.7
41.5
41.5
57.3
110.1

DETECT ARRAY

0.04400 0.14400 0.13600 0.18800 0.14800 0.13600 0.09200 0.06400

SEQUENCES

ROWS

PC ARRAY

0.8498
0.8189
0.7351
0.9702
0.9409
0.8374
0.9702
0.9455
0.8769

1
1
1
2
2
2
3
3
3

1
2
3
1
2
3
1
2
3

TABLE XI

NANCEE MAKEUP for Zig-Zag Pattern Example

NANCEE MAKEUP

RANGES ARRAY

0.0
9.4
10.9
11.7
22.2
25.2
25.5
110.1

DETECT ARRAY

0.0

0.04200 0.22400 0.25600 0.24000 0.20400 0.03400 0.0

PD ARRAY

0.8120
0.7969
0.7203
0.5000
0.6954
0.8038
0.9000
0.8778
0.8373

RCWS

1 1 1 2 2 2 3 3 3

SEQUENCES

1 2 3 1 2 3 1 2 3

TABLE XIII

NANCEE MAKEUP for TASDA AC Comparison

NANCEE OUTPUT

ROWS	SONOBUGYS	PU	ROWS	SONOBUGYS	PD	ROWS	SONOBUGYS	PD
1	1	0.2081	2	2	0.2304	3	3	0.2304
2	2	0.4033	4	4	0.4464	6	6	0.4464
3	3	0.5874	6	6	0.5480	12	12	0.5480
4	4	0.7513	8	8	0.8316	15	15	0.8316
5	5	0.7834	10	10	0.8694	18	18	0.8694
6	6	0.8130	12	12	0.9000	21	21	0.9000
7	7	0.8130	14	14	0.9000	24	24	0.9000
8	8	0.8130	16	16	0.9000	27	27	0.8999
9	9	0.8130	18	18	0.9000	30	30	0.8999
10	10	0.8130	20	20	0.9000			0.8998

PROGRAM INPUTS

PROCPLOSS CURVE
HEADING INFORMATION: 18144 DEPTH 8625 FT. FREQ .050 KHZ SEA STATE 3
FIGURE-OF-MERIT: 85.0 DB
SUBMARINE SPEED: 20 KNOTS
SUBMARINE COURSE: 0 DEGREES TRUE
SUBMARINE COURSE ACCURACY: 20 DEGREES EITHER SIDE OF COURSE
INITIAL SUBMARINE PROBABILITY AREA: X1= 10.0 X2= 10.0 X3= -10.0 X4= -10.0
Y1= -50.0 Y2= 50.0 Y3= -50.0 Y4= -50.0
TIME LATE: 3.3 HOURS
AIRCRAFT ON-STATION SPEED: 180 KNOTS
AIRCRAFT ON-STATION ALTITUDE: 20000 FEET

OPTIMUM PATTERN: 2 ROWS 12 SONOBUGYS - PROBABILITY-OF-DETECTION= 0.9000

1*	2*	3*	4*	5*	6*
7*	8*	9*	10*	11*	12*

OPTIMUM PATTERN PARAMETERS

ORIENTATION: 90/270 DEGREES TRUE
SONOBUOY SPACING: 30 NAUTICAL MILES
RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CENTER TO SONOBUOY PATTERN CENTER: 193.5 NAUTICAL MILES/ 0 DEGREES TRUE
MONITOR ALL PATTERN SONOBUGYS CONTINUOUSLY

TABLE XIV

NANCEE OUTPUT for TASDA AC Comparison

Both NANCEE and TASDA AC estimated the optimum pattern POD as 0.9. However, to compute these results TASDA AC executed in 1 minute and NANCEE executed in 20.89 seconds (with NRUNS and NRTOSS preset to 500).

The same program inputs were used again with TASDA AC except, this time, the number of submarine simulation runs for each probability calculation was increased to 50. Four optimum patterns were selected and each pattern's POD was near 0.95. The program execution time increased to 4 minutes 33.73 seconds.

VI. CONCLUSIONS

A. PROGRAM EFFECTIVENESS

NANCEE is well suited to determine which barrier type of sonobuoy pattern has the highest POD for a transiting nuclear submarine. The program executes rapidly, incorporates a high degree of realism, and is easy to use and understand. NANCEE MAKEUP and NANCEE OUTPUT are designed to provide sufficient program details to capitalize on the built-in flexibility of the MODE 1 and MODE 2 program functions.

B. COMPUTER REQUIREMENTS

Since NANCEE is coded in FORTRAN IV, the program must be used on computers equipped with a FORTRAN IV compiler. It is possible to convert NANCEE to the UNIVAC assembler language used in Tactical Support Center computers, but unfortunately, the program requires too much core to be used in the current P3C computer configuration. However, a proposed auxilliary drum storage addition to that computer would increase storage capacity sufficiently and make airborne use of the program feasible.

C. RECOMMENDATIONS FOR FUTURE EFFORT

Future effort with this program should be directed towards increasing program realism. Specifically, an adaption of the program to consider random monitor sequence disruption would be a significant

improvement. It is also feasible to adapt the program to consider random snorkel cycles (and therefore be appropriate for diesel submarines).

NANCEE is not intended to solve either holding or tracking submarine problems (see Chapter I). In fact, it is questionable whether the type of approach used in NANCEE is adaptable to these types of problems. Other computer programs such as TASDA and STEM can be used in these cases.

APPENDIX A
RADIO-FREQUENCY RANGE

The aircraft's altitude (ACALT), in feet, is used to compute the maximum radio-frequency range (RFRNG) in nautical miles.

The formula,

$$\text{RFRNG} = 1.064 \sqrt{\text{ACALT}},$$

defines this relationship. As ACALT increases, RFRNG also increases to an upper limit of about 120 nautical miles. No further increase is possible because of signal attenuation.

APPENDIX B

EXTENDED RADIO-FREQUENCY RANGE

The question of how large a sonobuoy pattern radius can be and still ensure adequate monitoring of all pattern sonobuoys is crucial. Obviously, if all pattern sonobuoys are within RFRNG of the center of the pattern, and if the aircraft orbits the center of the pattern, all sonobuoys are immediately available for monitoring no matter what monitor plan is chosen.

However, the radius of the pattern may be increased over RFRNG by capitalizing on the time sonobuoys will be left unmonitored during a monitor cycle. To demonstrate this, note that the aircraft can fly $CYCLE(I) \times ACSPD$ nautical miles during an I sequence monitor eye. Only one-half of that distancee ($(CYCLE(I) \times ACSPD)/2$) can be flown starting at and returning to the same position. If half of that distancee is distributed on one side of the pattern center and the other half on the other side, it appears that the sonobuoy pattern radius may be increased by,

$$\frac{CYCLE(I) \times ACSPD}{4} = \frac{I \times BMON \times ACSPD}{4} \quad \text{nautieal miles,}$$

Recall, however, that all pattern sonobuoys are to be monitored for a minimum of BMON hours per monitor cycle. With a pattern width of

$$RFRNG + \frac{I \times BMON \times ACSPD}{4} \quad \text{nautical miles,}$$

the sonobuoys farthest from pattern center fail to be monitored sufficiently. To correet this, the pattern radius should be reduced by $\frac{BMON \times ACSPD}{2}$ nautieal miles.

Based on this, a two-sequence monitor plan (I equals two) yields a maximum sonobuoy pattern radius of,

$$\text{RFRNG} + \frac{2 \times \text{BMON} \times \text{ACSPD}}{4} - \frac{\text{BMON} \times \text{ACSPD}}{2} = \text{RFRNG nautical miles.}$$

This leads to the unexpected conclusion that a two-sequence monitor plan allows a pattern radius only as large as RFRNG.

In comparison, a three sequence monitor plan (I equals three) yields a maximum pattern radius of,

$$\begin{aligned} & \text{RFRNG} + \frac{3 \times \text{BMON} \times \text{ACSPD}}{4} - \frac{\text{BMON} \times \text{ACSPD}}{2} \\ & = \text{RFRNG} + \frac{\text{BMON} \times \text{ACSPD}}{4} \text{ nautical miles.} \end{aligned}$$

Hence, $\text{RFRNG} + \frac{\text{BMON} \times \text{ACSPD}}{4}$ nautical miles is the extended radio-frequency range (ERFRNG) if a three sequence monitor plan is used.

APPENDIX C

GENERATION OF RANDOM DETECTION RANGES

As stated in Chapter III, the theory behind subroutine RANGE is that the propagation-loss curve varies in accordance with a normal distribution with a standard deviation of SIGMA decibels. In turn, this randomly varying propagation-loss curve is used to generate RUNNR random detection ranges.

Although it is theoretically correct to vary the propagation-loss curve and hold the figure-of-merit constant, in practice it involves far less numerical computations to use the opposite but equivalent procedure of holding the propagation-loss curve constant and varying the figure-of-merit normally. This is accomplished by using SIGMA and twelve uniform (0,1) random numbers, RN, to compute a random figure-of-merit deviation, FOMDEV, or

$$\text{FOMDEV} = \text{SIGMA} \times \left(\sum_{I=1}^{12} \text{RN}_I - 6.0 \right).$$

TEMPFM equals FOM + FOMDEV, and is a normally distributed random figure-of-merit with a mean of FOM and standard deviation of SIGMA.

A detection is defined to have occurred at a specified range from the sonobuoy where TEMPFM is larger than the value of the propagation-loss curve at that range. In a simulation run, a uniformly random range, IRANGE, between 0 and NPLPTS is selected. If the target is

detected at this first setting of IRANGE, that simulation run is disregarded. Otherwise, IRANGE is decreased in one-kiloyard increments until a detection occurs. In this manner, after NRUNS simulation runs, RUNNR random detection ranges are generated.

APPENDIX D

CALCULATION OF MEETING PROBABILITIES

Segment 2 was defined in Chapter III to be an area within a sonobuoy pattern zone for which the portion of the sonobuoy detection range a submarine must cross through is long enough to produce a minimum recognizable write-out, but less than the distance the submarine travels during the unmonitored portion of a monitor sequence. The POD of a submarine crossing a segment 2 area, p_Z , depends upon the success of the monitor cycle, and can be described as a meeting probability.

To compute these probabilities, consider an I sequence monitor cycle of $CYCLE(I)$ hours with a monitor time of $BMON$ hours per cycle and an unmonitor time of $UNMON(I)$ hours per cycle (where I equals two or three). A submarine will be within detection range of a sonobuoy in a segment 2 area for an average time of t hours, where $(6 \text{ minutes} < t < UNMON(I))$. Since t is less than $UNMON(I)$, t must also be less than $CYCLE(I)$. Therefore, the critical cycle in the computation of p_Z is the one during which the submarine passes through the sonobuoy detection range. If the start of monitoring (s) is allowed to vary uniformly between the start and end of a cycle (or from 0 to $CYCLE(I)$ hours) and, likewise, the entrance of the submarine into the sonobuoy's detection range (e) is varied uniformly between the start and end of the cycle, those cases where $BMON$ and t overlap are defined to mean that a detection has occurred. If $BMON$ and t do not overlap, there is no detection. The determination of the meeting probability for one

sonobuoy in a zone, then, is an equivalent problem to the determination of the probability that t and $BMON$ overlap.

The problem is divided into two cases:

Case 1 - The start of monitoring, s , occurs before the entrance of the submarine into the sonobuoy's detection range, e .

and,

Case 2 - The submarine enters the sonobuoy's detection range, e , before the start of monitoring, s .

For Case 1, a detection (overlap) occurs if $s - e < BMON$. Similarly, for Case 2, a detection occurs if $e - s < t$. These equations are plotted in Figure 4. Inside the square of Figure 4, the shaded area is the area where an overlap will occur, and hence, is the area where the submarine will be detected. The unshaded area is the area where no detection will occur. The shaded area divided by the area of the square (i.e. $CYCLE(I)^2$) is p_S , the probability a sonobuoy monitored $BMON$ hours per cycle, with I sequences per cycle, will detect a submarine passing through a segment 2 area of a zone.

Depending upon the number of rows in a sonobuoy pattern zone, there may be more than one sonobuoy in that zone with a segment 2 area. Fortunately, for a given sonobuoy detection range, if more than one sonobuoy has a segment 2 area, each has the same average detection-range-crossing-time, t . Hence the meeting probabilities, p_S , for each of the sonobuoys are the same. Prior to the first detection, sonobuoy detections are independent events and can be thought of as independent Bernoulli trials. The probability that at least one of n sonobuoys, in a segment 2 area of a zone will detect the submarine, is the following sum of binomial probabilities:

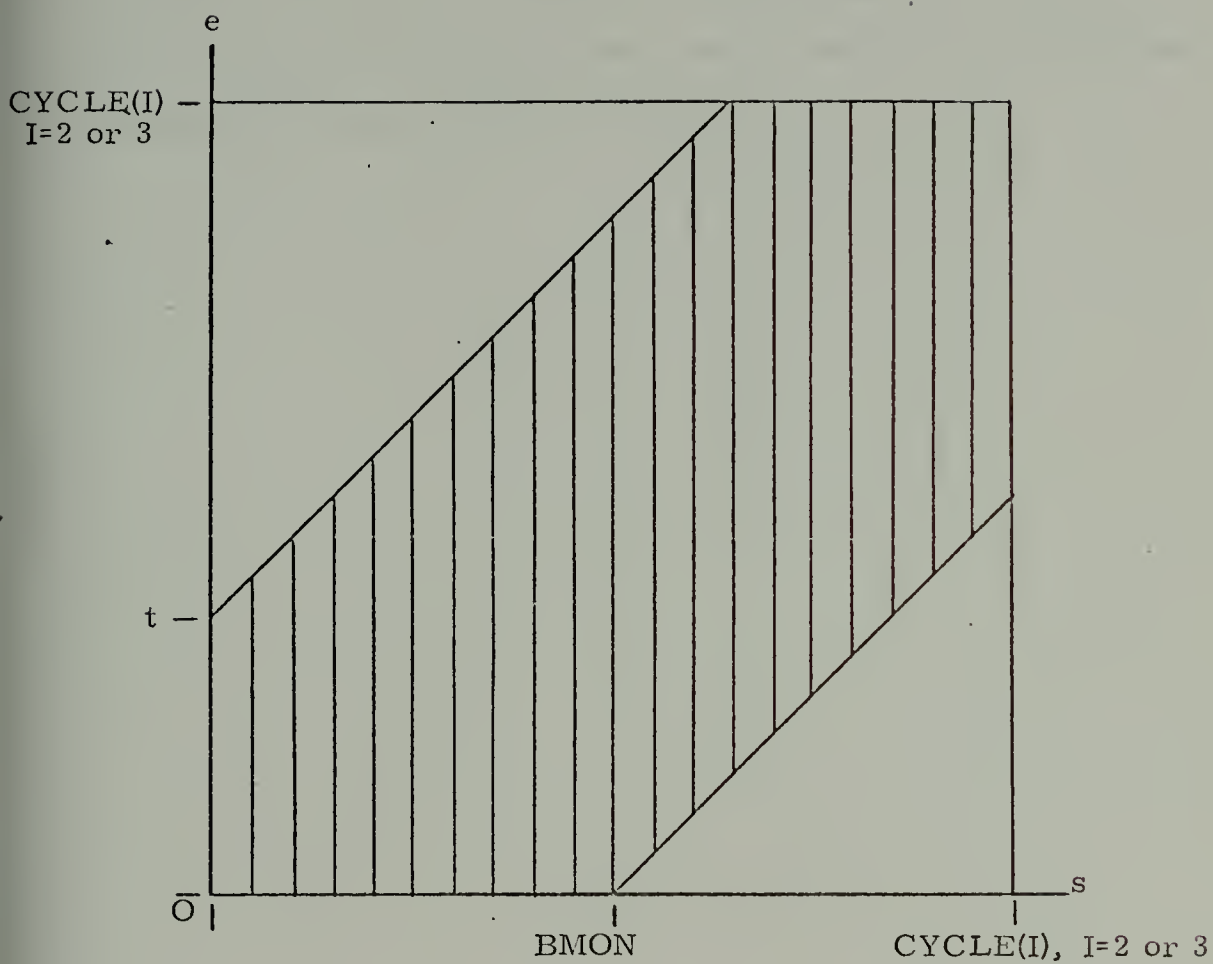


Figure 4
Meeting Probability Graph

$$p_Z = \sum_{I=1}^n \binom{n}{I} p_S^I (1 - p_S)^{n-I}.$$

p_Z is the Segment 2 meeting probability for the zone.

It must be noted that the discussion above is somewhat simplified in an attempt to make the idea of meeting probability clear. Actual segment 2 areas are the DISTM1 and DISTM2 spanned areas of Figures 7, 8, and 9. The average crossing distances through these areas are HTM1 and HTM2 respectively.



APPENDIX E

PROGRAM INPUTS

Table XV lists the variables and arrays that require initialization in the program, along with their associated data card number, range, and meaning (also, recall that Appendix F contains more comprehensive definitions of all major program variables and arrays).

In amplification of Table XV, if MODE equals 2, IBOYSP and IBMON are input to the program on data card number 1a. However, if MODE equals 1, IBOYSP and IBMON are computed in subroutine GEOM and card 1a must not be included in the data deck.

Furthermore, as stated in Chapter III, the initial submarine probability area must be a rectangle and it is input to the program by virtue of data card number 4. (X1, Y1) and (X2, Y2) are any two distinct, adjacent corners of the initial submarine probability area (i.e. at opposite ends of a common side of the rectangle).

Finally, data cards 7 through 33 contain propagation-loss curve heading information followed by the propagation-loss curve in decibels discretized into one-kiloyard increments. The number of one-kiloyard increments used by the program out to a maximum of 250 kiloyards is specified by NPLPTS. Normally it should not be necessary to keypunch any of cards 7 through 33. Instead, it is intended that they be punched by Fleet Numerical Weather Central Monterey's passive sonar prediction program.

Data Card Nr	Variable/Array	Units	Range	Meaning
1	MODE	-	1 or 2	Program MODE
1a	IBOYSP	NM	4 - 200	sonobuoy spacing
1a	IBMON	Mins	10 - 60	sonobuoy monitor time per sequence
2	IACSPD	KTS	120 - 350	on-station aircraft speed
2	IACALT	FT	100 - 30,000	on-station aircraft altitude
3	ISUBSPD	KTS	3 - 50	estimated submarine speed
3	ISUBCUS	DEG T	000 - 360	estimated submarine course
3	ICUSAC	DEG	000 - 180	estimated submarine course accuracy
4	X1	NM	$\left\{ \begin{array}{l} \text{no side of} \\ \text{initial sub-} \\ \text{marine prob-} \\ \text{ability area} \\ \text{longer than 1000NM} \end{array} \right\}$	$\left. \begin{array}{l} (X1, Y1) \text{ and } (X2, Y2) \\ \text{are adjacent corners} \\ \text{of the initial submarine} \\ \text{probability area.} \end{array} \right\}$
4	Y1	NM		
4	X2	NM		
4	Y2	NM		
5	TLATE	HRS	0 - 48	time late
6	FOM	DB	0 - 220	figure-of-merit
6	NPLPTS	Kiloyards	0 - 250	number of propagation-loss points
7, 8	IDATA-(Array)	-	-	propagation-loss curve identification data
9-33	PLOSS-(Array)	DB	0 - 220	propagation-loss curve

TABLE XV

Program Inputs

APPENDIX F

LIST OF MAJOR PROGRAM VARIABLES AND ARRAYS

- ACALT - The aircraft's on-station altitude in feet above sea level.
- ACSPD - The aircraft's on-station speed in knots.
- ALFA - See Figure 5.
- AX1 - Absolute value of X1.
- AX2 - Absolute value of X2.
- AY1 - Absolute value of Y1.
- AY2 - Absolute value of Y2.
- BMON - The sonobuoy monitor-time-per-sequence, in hours.
- BSUM - Used to generate the vector array PY. It is varied from 0 to $2.0 \times \text{SHIFT}$ in increments of BUOYSP.
- BUOYD - In the TOSS subroutine, the distance from the current submarine position (TEMPX, TEMPY) to the sonobuoy positions (PCX, PY(I)), where I varies from 1 to NRBUOY.
- BUOYSP - The sonobuoy pattern spacing in nautical miles.
- CIRMAX - The maximum distance, in nautical miles, from the center of the sonobuoy pattern area at which a detection can be expected. $\text{CIRMAX} = \text{RANGES}(\text{INDEX}) + \text{SHIFT}$.
- CUSACC - The maximum angle in degrees that the submarine is expected to deviate to either side of its projected course.
- CYCLE(I) - If a sonobuoy pattern is monitored with I sequences per eyele, where I equals two or three, CYCLE(I) is the time in hours to complete one cycle.
- DETECT(I) - A vector array containing the probabilities that a submarine will pass through sonobuoy pattern zone I, where I varies from 1 to NRBUOY.
- DETS(I) - A vector array containing the number of detections which occurred at range I in the RANGE subroutine, where I varies from 1 to NPLPTS.

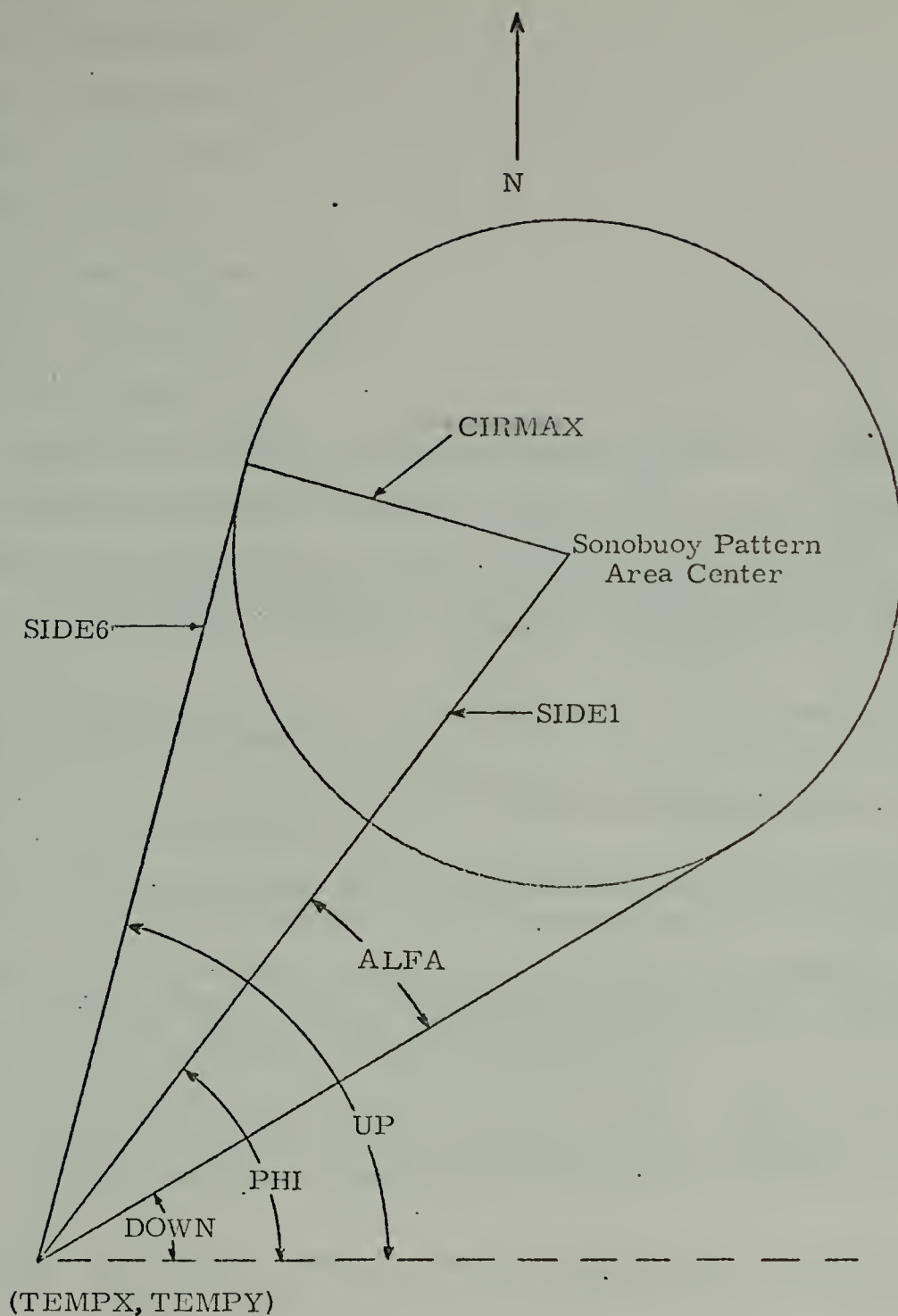


Figure 5

Geometry used to Calculate Whether TEMCUS Penetrates Sonobuoy Pattern Detection Range

DIST1 - See Figure 6.

DIST2 - See Figure 6.

DISTB - See Figure 8.

DISTI - See Figure 10.

DISTM1 - See Figures 7 and 8.

DISTM2 - See Figures 8 and 9.

DOWN - See Figure 5.

DX - One-half the distance between the points (XO, YO) and (XP, YP).

DY - One-half the distance between the points (-XO, -YO) and (XP, YP).

ERFRNG - The extended radio-frequency range if a three sequence monitor plan is used, with a sonobuoy monitor time per cycle of BMON. $ERFRNG = RFRNG + \frac{BMON \times ACSPD}{4}$ (see Appendix B).

FILL1 - A working variable set to $0.05 \times SUBSPD$ to avoid unnecessary repeat calculations.

FILL2 - A working variable set to $SPACE/2.0$ to avoid unnecessary repeat calculations.

FILL3 - A working variable set to $(UNMON(I) \times SUBSPD)/2.0$, where I equals two or three, to avoid unnecessary repeat calculations.

FLAG - A logical variable used during the computation of pattern probabilities. For a fixed number of pattern rows, FLAG equals .FALSE. until the first occurrence of a three sequence monitor cycle. Thereafter, FLAG equals .TRUE..

FOM - The figure-of-merit of the submarine target. FOM equals $SL - AN - RD$, where SL is the target source level, AN is the ocean ambient noise level, and RD is the operator recognition differential.

FOMDEV - The figure-of-merit deviation computed as a random normal deviation about a mean of zero and a standard deviation of SIGMA.

GAMMA - The angle to which the point (RX, RY) must be rotated so that a single row sonobuoy pattern oriented perpendicular to ISUBCS is rotated about the center of the initial submarine probability area to a north/south orientation east of the center of the initial submarine probability area.

GCOS - The cosine of the angle GAMMA.

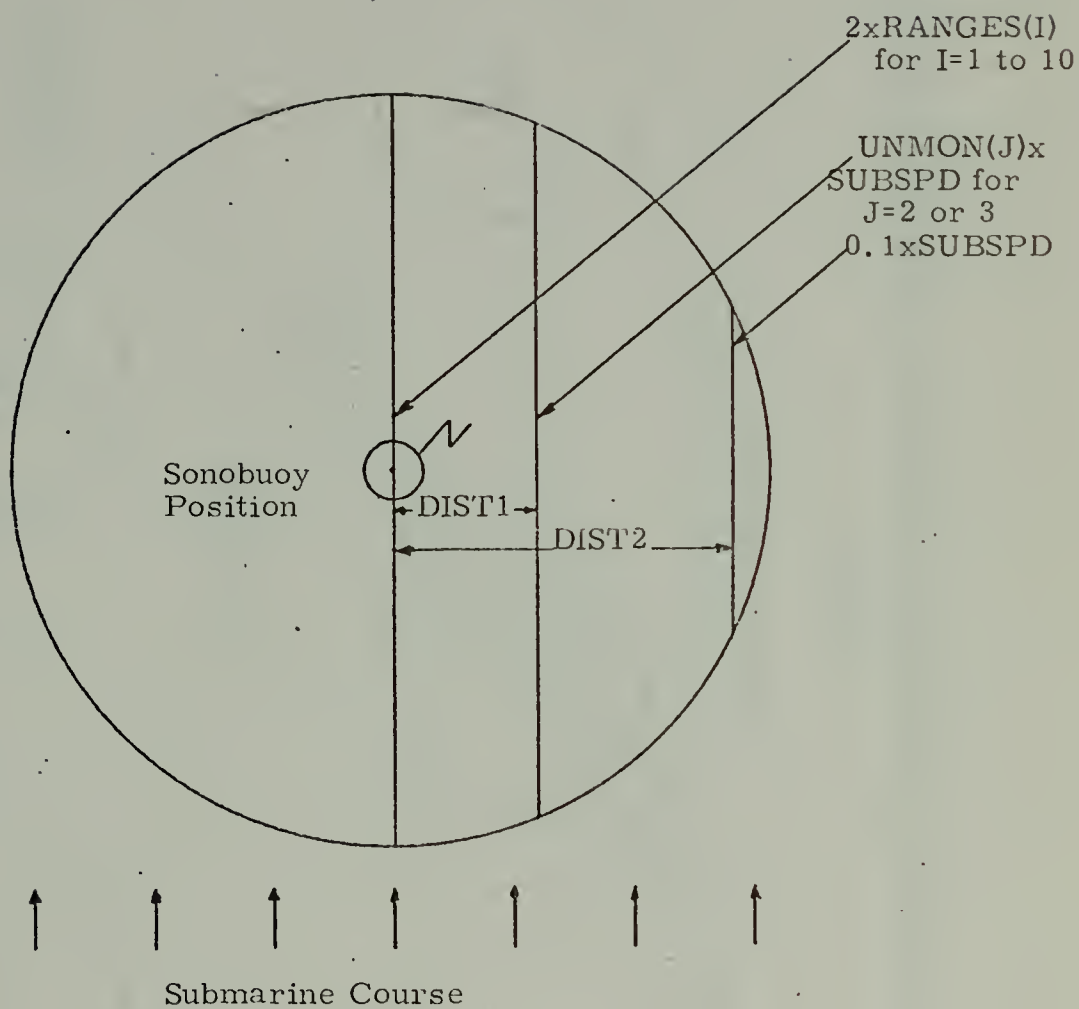


Figure 6

Sonobuoy Detection Range Penetration Areas DIST1 and DIST2

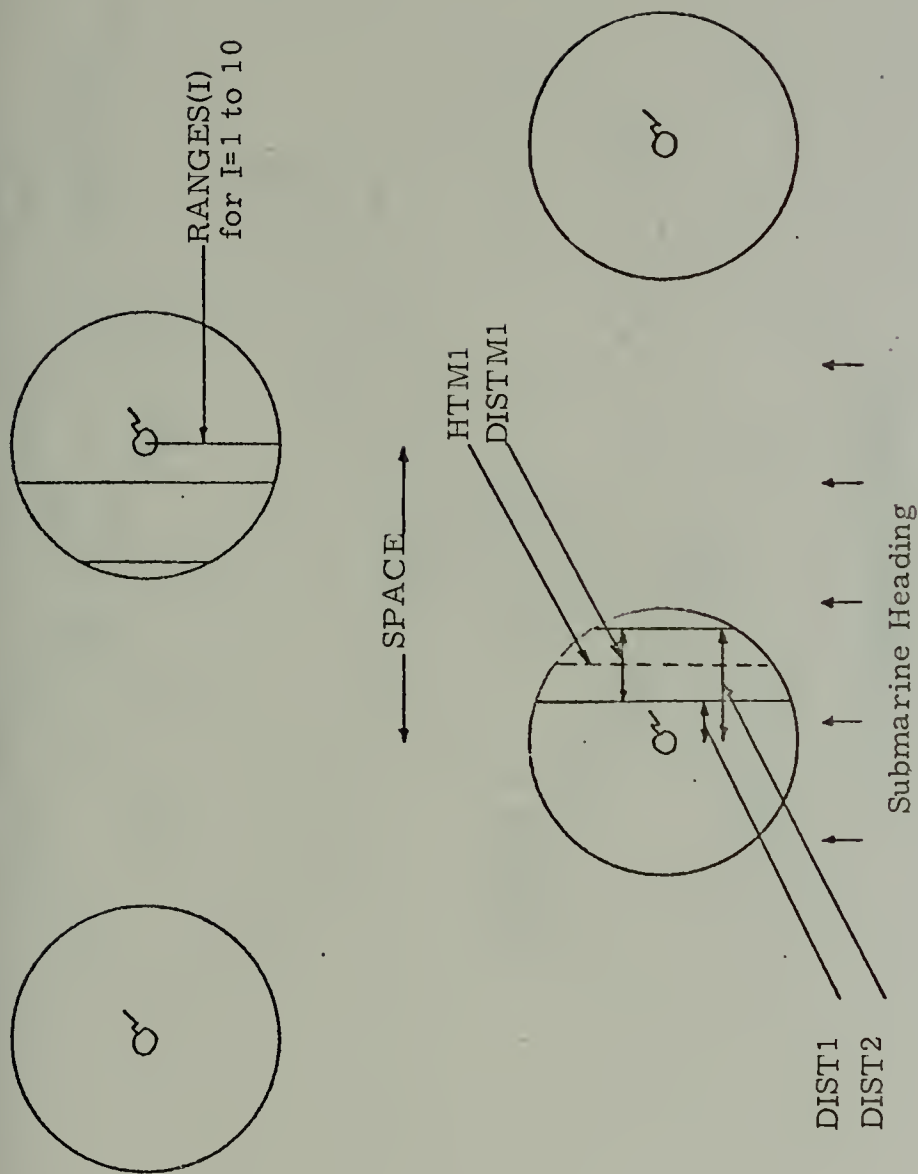


Figure 7

Two-Row Sonobuoy Pattern Detection Range Penetration Arrangement if $DIST2 \leq SPACE/2.0$

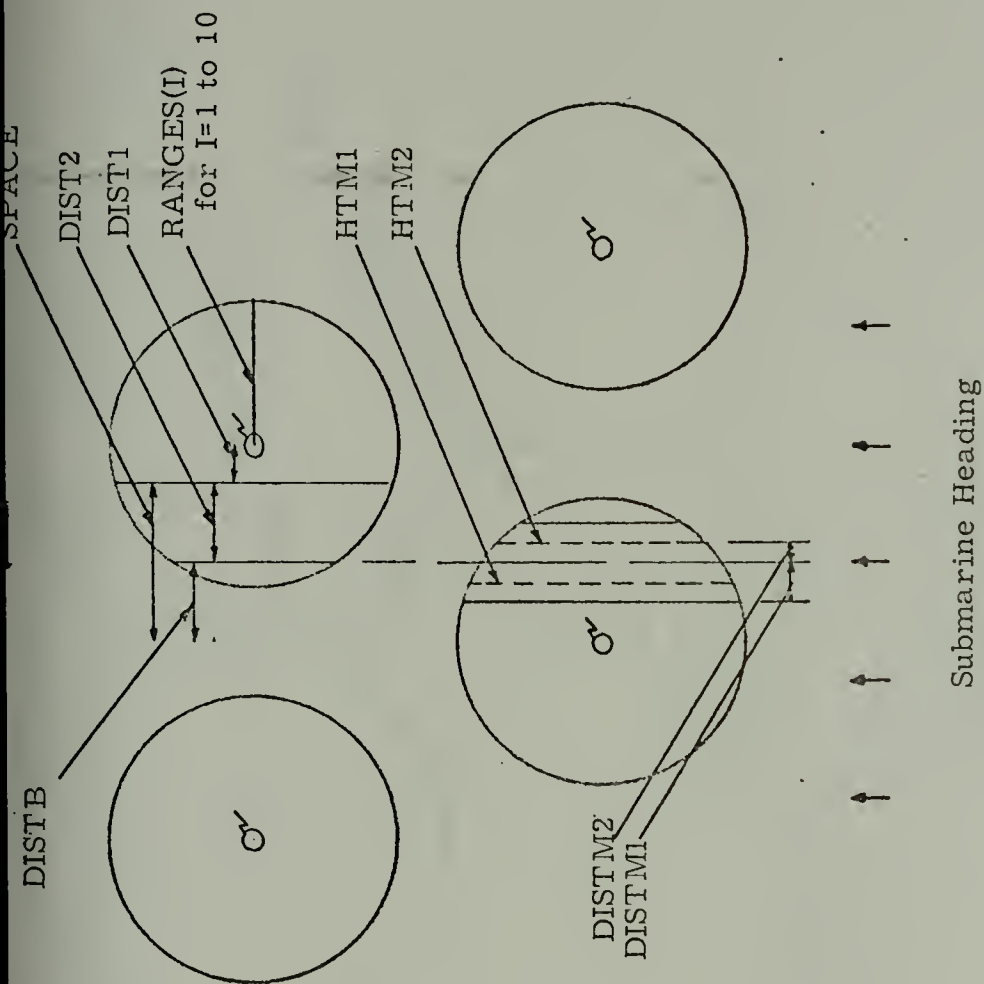


Figure 8

Two-Row Sonobuoy Pattern Detection Range Penetration Arrangement if $DIST2 > SPACE/2.0$
and $DIST1 + DIST2 \leq SPACE$

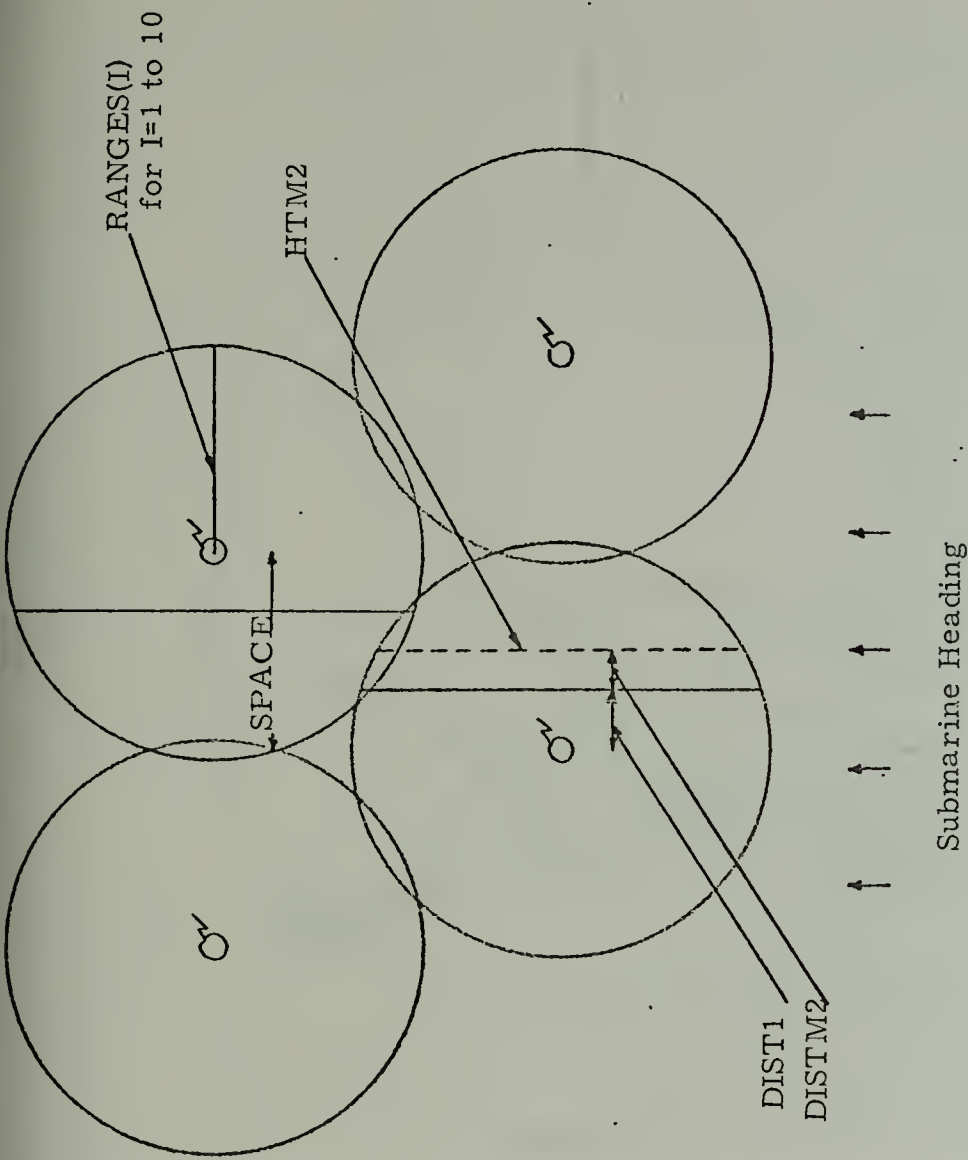


Figure 9

Two-Row Sonobuoy Pattern Detection Range Penetration Arrangement if $DIST2 > SPACE/2.0$ and $DIST1 + DIST2 > SPACE$

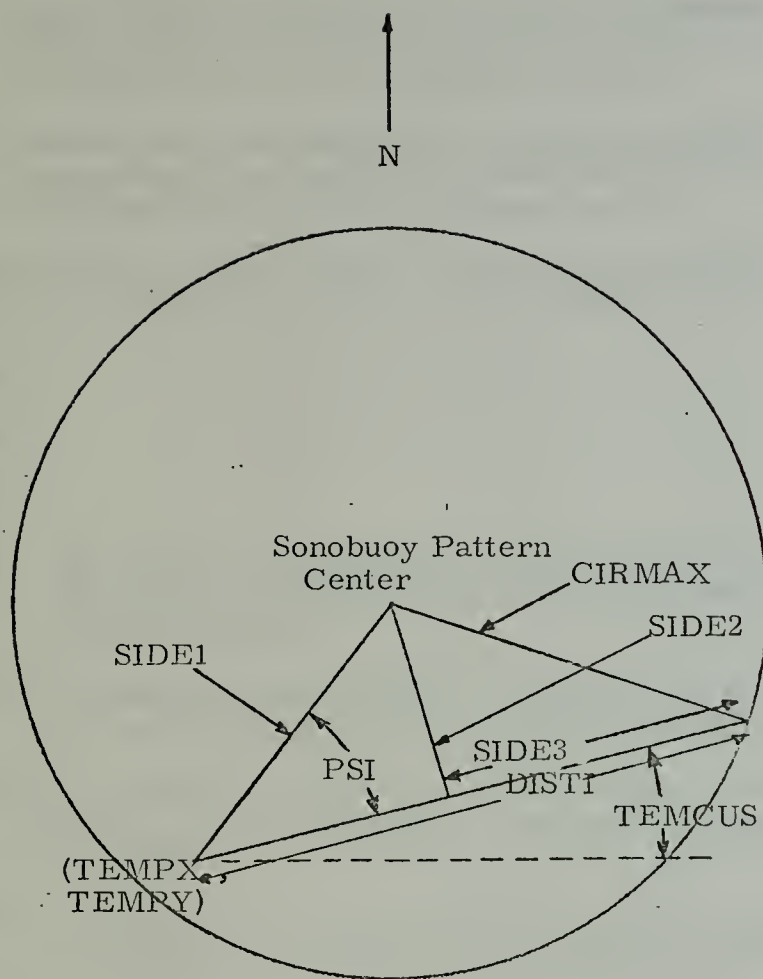


Figure 10

Toss Subroutine Arrangement at Start of Submarine Simulation Run
if $SIDE1 \leq CIRMAX$

GSIN - The sine of the angle GAMMA.

HT1 - With HT2, working variables used to compute HTM1 and HTM2.

HT2 - See HT1.

HTM1 - The average sonobuoy-detection-range-distance which a submarine must cross if a sonobuoy pattern zone is penetrated at a DISTM1 area. See Figures 7 and 8.

HTM2 - The average sonobuoy-detection-range-distance which a submarine must cross if a sonobuoy pattern zone is penetrated at a DISTM2 area. See Figures 8 and 9.

I1 - With LSIDE, MSIDE, I2, I3, and I4, zone pointers for construction of three monitor sequence pattern probabilities.

I2 - See I1.

I3 - See I1.

I4 - See I1.

IACALT - An integer representation of the aircraft's on-station altitude in feet above sea level. It is used for program input/output purposes.

IACSPD - An integer representation of the aircraft's on-station speed in knots. It is used for program input/output purposes.

IBMON - An integer representation of the sonobuoy monitor time per monitor cycle in minutes. It is used for program input/output purposes.

IBOYSP - An integer representation of the sonobuoy pattern spacing in nautical miles. It is used for program input/output purposes.

ICUSAC - An integer representation of the maximum angle in degrees, that the submarine is expected to deviate to either side of its projected course. It is used for program input/output purposes.

ICYCL - The number of sequences per monitor cycle computed for the optimum sonobuoy pattern.

IDATA(I) - An integer array used to store propagation-loss curve identification data.

INCR - In the TOSS subroutine, a computed number of two nautical mile increments along which the submarine has the potential to be detected by the sonobuoy pattern.

INDEX - Defines which element of the RANGES array will be used to represent the average detection range (i.e. average detection range equals RANGES(INDEX)). Preferably, RANGES(INDEX) should equal the middle-sized range, or RANGES(5). However, to prevent the average detection range from being zero, INDEX equals I where I is the first integer larger than 4 but less than 11 such that a submarine crossing through the center of RANGES(I) is detectable for at least six minutes (minimum recognizable write-out time).

INNER - For a sonobuoy pattern monitored with a three sequence monitor plan, the number of sonobuoy pattern zones that make up one monitor sequence.

INSIDE - The maximum number of sonobuoys that can be lined up in a single row with a spacing equal to IBOYSP and still fit inside RFRNG.

IOREN1 - With IOREN2 used to construct the orientation of the optimum sonobuoy pattern in degrees true.

IOREN2 - See IOREN1.

IRANGE - A random range of the simulated submarine from a sonobuoy in the RANGE subroutine. IRANGE is decreased in one-kiloyard increments until a detection is made.

ISEED - Used as a seed for the random number generating subroutine RANDOM. ISEED must be a positive integer between 1 and 2147483647 and should be changed periodically to ensure program randomness.

ISUBCS - An integer representation of the submarine's expected course in degrees true. It is used for program input/output purposes.

ISUBSP - An integer representation of the submarine's expected speed in knots. It is used for program input/output purposes.

LINES - The number of rows in the optimum sonobuoy pattern.

LSIDE - With MSIDE, sonobuoy pattern zone pointers used when constructing sonobuoy pattern probabilities.

MAX - With MIN the extreme end sonobuoy pattern zones during the initial construction of a three-monitor-sequence probability.

MID - The middle zone of a sonobuoy pattern during the initial construction of a three-monitor-sequence probability.

MIN - See MAX.

MISS - In the TOSS subroutine, those of the NRTOSS submarine simulations which failed to be detected by the sonobuoy pattern.

MODE - A program input parameter which designates the program mode. If MODE equals 1, IBOYSP and IBMON are computed in the GEOM subroutine. If MODE equals 2, IBOYSP and IBMON must be input to the program.

MSIDE - See LSIDE.

NPLPTS - The number of propagation-loss curve points used by the RANGE subroutine to compute the RANGES vector array.

NRBUOY - The maximum number of sonobuoys that can be lined up in a single row with a spacing of IBOYSP and still fit inside ERFNG.

NRTOSS - The number of submarine simulation runs that are made through the sonobuoy pattern area in the TOSS subroutine.

NRUNS - The number of runs used to generate the RANGES vector array in the RANGE subroutine.

NSONO - The total number of sonobuoys in the optimum sonobuoy pattern.

NSONO1 - A variable which contains the total number of sonobuoys in one-row patterns.

NSONO2 - A variable which contains the total number of sonobuoys in two-row patterns.

NSONO3 - A variable which contains the total number of sonobuoys in three-row patterns.

NSROW - A variable containing the number of sonobuoys in each row of the optimum sonobuoy pattern.

NVEC - Used in the call to subroutine RANDOM to designate how many uniform (0, 1) random numbers are to be generated.

OP - The sonobuoy pattern probabilities.

PART2 - The average probability that a monitor plan consisting of I sequences (where I equals two or three) will detect a submarine passing through a DISTM1 area of a sonobuoy pattern zone at SUBSPD knots, given that the detection range is a member of the RANGES vector array.

PART3 - The average probability that a monitor plan consisting of I sequences (where I equals two or three) will detect a submarine passing through a DISTM2 area of a sonobuoy pattern zone at SUBSPD knots, given that the detection range is a member of the RANGES vector array.

PCOS - The cosine of the angle PSI.

PCX - The distance in nautical miles from the center of the initial submarine probability area to the center of the sonobuoy pattern area. It is also the horizontal component of the row of sonobuoys in the TOSS subroutine.

PD(I, J) - An array which contains the zone detection probabilities. PD(I, J) is the probability an I row zone being monitored with J sequences of BMON hours per monitor cycle will detect a submarine passing through the zones. The PD array is used with the DETECT vector array to construct pattern probabilities in the BUILD subroutine.

PHI - See Figure 5.

PI - A numerical constant initialized to 3.14159.

PLOSS(I) - A vector array which contains the propagation-loss curve, in decibels, (discretized into one kiloyard increments) out to a maximum of 250 kiloyards.

PMAX - The maximum POD found after searching through all one, two, and three row sonobuoy pattern probabilities out to a maximum pattern radius of ERFRNG.

PROB - The zone POD for a particular monitor plan, number of sonobuoy pattern rows, and sonobuoy detection range (particular value of the RANGES vector array).

PSI - See Figures 10 and 11.

PSIN - The sine of the angle PSI.

PSUM - A working variable used to sum ten values of PROB. For each summation step, the pattern rows and monitor plan are fixed, but RANGES(I) varies from I equals 1 to 10. When the summation is complete, PSUM divided by 10 is entered into the PD vector array.

PVEC(I, J) - The POD for I row sonobuoy pattern which consists of J zones.

PY(I) - A vector array which contains the vertical components of the single row of sonobuoys in the TOSS subroutine.

RANGES(I) - A vector array containing 10 equally likely expected sonobuoy detection ranges from the smallest to the largest. Theoretically, a submarine operating at a distance of RANGES(I) (where I varies from 1 to 10), from a sonobuoy will be detected (100 - Ix10) percent of the time.

RFRNG - The maximum radio-frequency range, in nautical miles (see Appendix A).

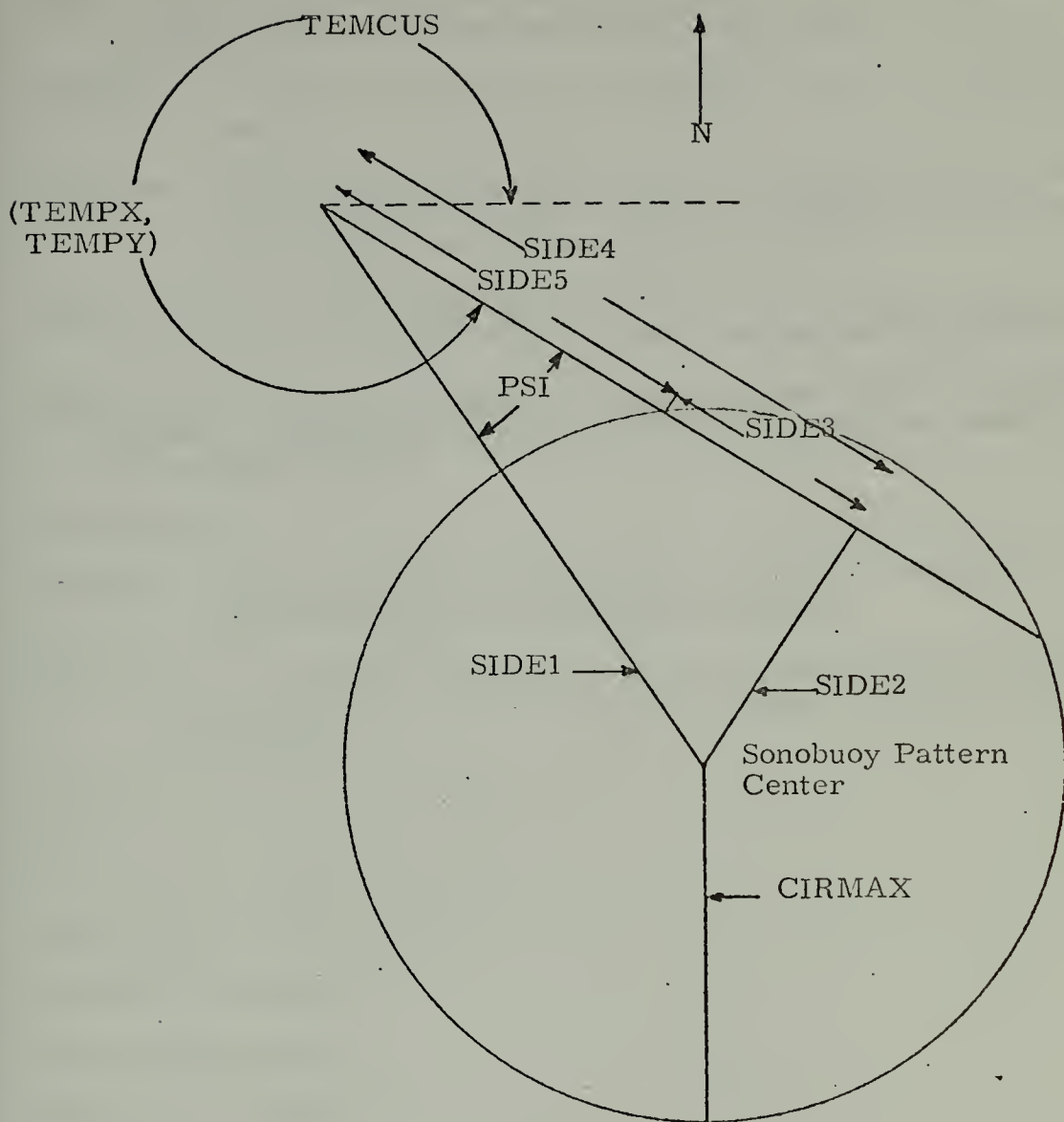


Figure 11

TOSS Subroutine Arrangement at Start of Submarine Simulation Run
if $SIDE1 > CIRMAX$

RN(I) - A vector array used to store NVEC uniform (0, 1) random numbers generated by the RANDOM subroutine.

RNGSSQ - A working variable set to $RANGES(I)^2$ where I is between 1 and 10.

RNGSUM - A working variable used to sum the elements of the DETS(I) vector array, as I varies from 1 to RUNNR. In the process, the RANGES vector array is generated.

RNSUM - A working variable used to sum twelve random numbers used in the computation of the normal random variable FOMDEV.

RX - With RY defines a uniformly random position inside a rectangle similar to the initial submarine probability area but rotated to an upright position.

RY - See RX.

RUNNR - The number of random detection ranges generated in the RANGE subroutine (out of NRUNS trials).

SHIFT - The maximum radius of a one-row sonobuoy pattern which fits inside the limits of ERFRNG and has a sonobuoy spacing of IBOYSP.

SIDE1 - See Figures 10 and 11.

SIDE2 - See Figures 10 and 11.

SIDE3 - See Figures 10 and 11.

SIDE4 - See Figure 11.

SIDE5 - See Figure 11.

SIDE6 - See Figure 5.

SIGMA - A normal distribution standard deviation for the propagation-loss profile.

SPACE - In the MEET subroutine, SPACE is equal to BUOYSP when the number of sonobuoy pattern rows is one, and SPACE equals BUOYSP/2.0 when there are two or three sonobuoy pattern rows.

SQMXCR - The square of CIRMAX.

SUBCUS - The submarine's expected course in degrees true.

SUBSPD - The submarine's expected speed in knots.

TCOS - The cosine of the angle TEMCUS.

- TEMCUS - The submarine course during a simulation run in the TOSS subroutine. TEMCUS varies uniformly between the limits of ICUSAC with a mean of 000 degrees.
- TEMPFM - The temporary figure-of-merit computed as a random normal deviation about a mean of FOM and a standard deviation of SIGMA. $TEMPFM = FOM + FOMDEV$.
- TEMPX - With TEMPY, defines the temporary position of the simulated submarine in the TOSS subroutine as it proceeds toward and through the sonobuoy pattern area.
- TEMPY - See TEMPX.
- THETA - The orientation of the initial submarine probability area. See Figure 12.
- TLATE - The time that elapses between the fixing of the initial submarine probability area and the aircraft's arrival on station.
- TSIN - The sine of the angle TEMCUS.
- UNMON(I) - The unmonitored portion of an I sequence monitor cycle in hours.
- UP - See Figure 5.
- X1 - With Y1 defines one corner of the initial submarine probability area. X1 is the horizontal distance in nautical miles from that corner to a north/south line through the center of the initial submarine probability area. If the corner is to the left of the north/south line X1 has negative value. Otherwise, X1 is positive.
- X2 - With Y2, defines a corner of the initial submarine probability area which is distinct from (X1, Y1), (X3, Y3), and (X4, Y4). The point (X2, Y2) is constructed in a manner similar to the construction of the point (X1, Y1).
- X3 - With Y3, defines a corner of the initial submarine probability area which is distinct from (X1, Y1), (X2, Y2), and (X4, Y4). The point (X3, Y3) is constructed in a manner similar to the construction of the point (X1, Y1).
- X4 - With Y4, defines a corner of the initial submarine probability area which is distinct from (X1, Y1), (X2, Y2), and (X3, Y3). The point (X4, Y4) is constructed in a manner similar to the construction of the point (X1, Y1).

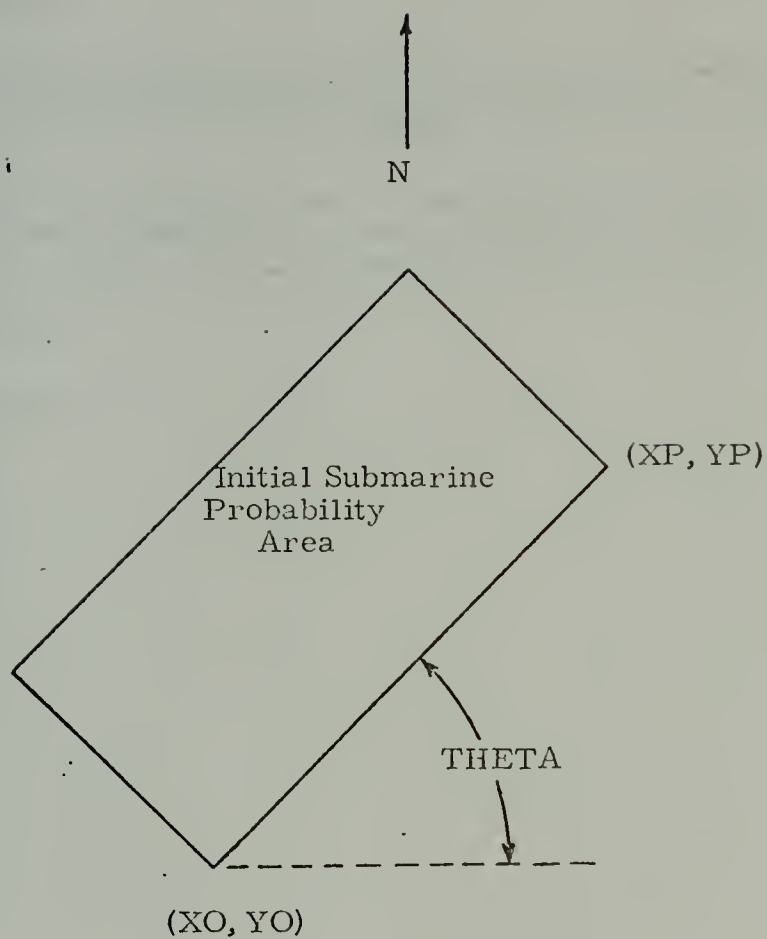


Figure 12

Initial Submarine Probability Area

- Y1 - With X1 defines one corner of the initial submarine probability area. Y1 is the vertical distance in nautical miles from that corner to an east/west line through the center of the initial submarine probability area. If the corner below the east/west line Y1 has negative value. Otherwise, Y1 is positive.
- Y2 - See X2.
- Y3 - See X3.
- Y4 - See X4.
- XO - With YO, defines either the southern-most corner of the initial submarine probability area, or if there is a tie, the southwest corner of the initial submarine probability area (see Figure 12).
- XP - With YP, defines either the eastern-most corner of the initial submarine probability area, or if there is a tie, the southeast corner of the initial submarine probability area (see Figure 12).
- YO - See XO.
- YP - See XP.

NANCEE COMPUTER PROGRAM LISTING

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C      CMMCN MODE, BMON, IBMON, ACSPD, SUBSPD, SUBCUS, CUSACC, IACSPD, IACALT, ISCARD00001
C      1UBSP, 1SUBCS, ICUSAC, TPLATE, FOM, BUGYSP, IBOYSP, NPLPTS, INSIDE, INDEX, X1, CARD00002
C      2Y1, X2, Y2, DX, DY, RFRNG, NRBUOY, SHIFT, THETA, PCX, ICYCL, LINES, NSONO, PMAXCARG0003
C      3, PLOSS(250), RANGES(10), PY(150), DETECT(150), UNMON(3), CYCLE(3), PD(3, CARD00004
C      43), PVEC(3, 48), IDATA(40) CARD00005
C      READ AND TEST PROGRAM INPUTS. CARD00006
C      DATA PI/3.14159/ CARD00007
C      READ PROGRAM MODE. CARD00008
C      READ(5, 800) MODE CARD00009
C      800 FORMAT(3I10) CARD00010
C      IF((MODE.EQ.1).OR.(MODE.EQ.2)) GO TO 10 CARD00011
C      WRITE(6, 900) CARD00012
C      900 FORMAT(10) EXECUTION TERMINATED. INPUT PROGRAM MODE DOES NOT EQ CARD00013
C      1VAL 1 OR 2.' CARD00014
C      GO TO 9000 CARD00015
C      10 IF(MODE.EQ.1) GO TO 20 CARD00016
C      IF THE PROGRAM MODE IS 2, READ THE SONOBUOY SPACING AND SONOBUOY CARD00017
C      MONITOR TIME. CARD00018
C      READ(5, 800) IBOYSP, IBMON CARD00019
C      BUGYSP = IBOYSP CARD00020
C      BMON = IBMON/60.0 CARD00021
C      IF((BUGYSP.GE.4).AND.(BUOYSP.LE.200)) GO TO 30 CARD00022
C      WRITE(6, 910) EXECUTION TERMINATED. INPUT SONOBUOY SPACING OUTSIDE CARD00023
C      910 FORMAT(10) LIMITS 4 TO 200 NM.' CARD00024
C      1 LIMITS 4 TO 200 NM.' CARD00025
C      GO TO 9000 CARD00026
C      30 IF((BMON.GE.0.166666).AND.(BMON.LE.1.0)) GO TO 20 CARD00027
C      WRITE(6, 920) EXECUTION TERMINATED. INPUT SONOBUOY MONITOR TIME OUT CARD00028
C      920 FORMAT(10) LIMITS 10 TO 60 MINUTES.' CARD00029
C      1 LIMITS 10 TO 60 MINUTES.' CARD00030
C      GO TO 9000 CARD00031
C      READ AIRCRAFT ON-STATIC SPEED AND ALTITUDE. CARD00032
C      20 READ(5, 800) IACSPD, IACALT CARD00033
C      ACSPD = IACSPD CARD00034
C      ACALT = IACALT CARD00035
C      IF((ACSPD.GE.120).AND.(ACSPD.LE.350)) GO TO 40 CARD00036
C      WRITE(6, 930) CARD00037
C      CARD00038
C      CARD00039
C      CARD00040
C      CARD00041
C      CARD00042
C      CARD00043
C      CARD00044
C      CARD00045

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930 FORMAT('O EXECUTION TERMINATED. INPUT ACFT AIRSPEED OUTSIDE LIMITS 120 TO 350 KTS.')
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CARD00046
CARD00047
CARD00048
CARD00049
CARD00050
CARD00051
CARD00052
CARD00053
CARD00054
CARD00055
CARD00056
CARD00057
CARD00058
CARD00059
CARD00060
CARD00061
CARD00062
CARD00063
CARD00064
CARD00065
CARD00066
CARD00067
CARD00068
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CARD00093

```

1 GO TO 9000
40 IF((ACALT.GE.100).AND.(ACALT.LE.30000)) GO TO 50
WRITE(6,940)
940 FORMAT('O EXECUTION TERMINATED. INPUT ACFT ALTITUDE OUTSIDE LIMITS 100 TO 30,000 FT.')
```

CARD00052
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CARD00093

```

1 GO TO 9000
50 RFRNG = 1.064*SQRT(ACALT)
IF(RFRNG.GT.120) RFRNG = 120.0

C
C
C
READ THE SUBMARINE'S SPEED, COURSE, AND COURSE ACCURACY.

READ(5,800) ISUBSP,ISUBCS,ICUSAC
SUBSPD = ISUBSP
SUBCUS = ISUBCS
CUSACC = ICUSAC
IF((SUBSPD.GE.3).AND.(SUBSPD.LE.50)) GO TO 60
WRITE(6,950)
950 FORMAT('O EXECUTION TERMINATED. INPUT SUB SPEED OUTSIDE LIMITS 13 TO 50 KTS.')
```

CARD00052
CARD00053
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CARD00092
CARD00093

```

1 GO TO 9000
60 IF((SUBCUS.GE.0).AND.(SUBCUS.LE.360)) GO TO 70
WRITE(6,960)
960 FORMAT('O EXECUTION TERMINATED. INPUT SUB COURSE OUTSIDE LIMITS 0 TO 360 DEGREES.')
```

CARD00052
CARD00053
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CARD00091
CARD00092
CARD00093

```

1 GO TO 9000
70 SUBCUS = SUBCUS*PI/180.0
IF((CUSACC.GE.0).AND.(CUSACC.LE.180)) GO TO 80
WRITE(6,970)
970 FORMAT('O EXECUTION TERMINATED. INPUT CCOURSE ACCURACY OUTSIDE LIMITS 0 TO 180 DEGREES.')
```

CARD00052
CARD00053
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CARD00091
CARD00092
CARD00093

```

1 GO TO 9000
80 CUSACC = CUSACC*PI/180.0

C
C
C
READ TWO ADJACENT CORNERS OF THE INITIAL SUBMARINE PROBABILITY AREA.

READ(5,810) X1,Y1,X2,Y2
FCRMT(4F10.1)
IF(((X1 - X2)**2 + (Y1 - Y2)**2).GE.1000000) GO TO 90
IF(((X1 + X2)**2 + (Y1 + Y2)**2).LT.1000000) GO TO 100
WRITE(6,980)
980 FORMAT('O EXECUTION TERMINATED. INPUT INITIAL PROBABILITY AREA 1 HAS ONE SIDE LONGER THAN 1000 NM.')
```

CARD00052
CARD00053
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CARD00085
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CARD00090
CARD00091
CARD00092
CARD00093

```

1 GO TO 9000
READ TIME-LATE.

C
C
C
```



```

100 READ(5,810) TLATE
   IF((TLATE-GE.0).AND.(TLATE.LE.48)) GO TO 110
   WRITE(6,990)
990 FFORMAT(10) EXECUTION TERMINATED. INPUT TIME LATE OUTSIDE LIMITS
   1 0 TO 48 HOURS.
   GC TO 9000
C
C
C
110 READ(5,820) FOM,NPLPTS
820 FFORMAT(10,1,110)
   IF((FOM-GE.0).AND.(FOM.LE.220)) GO TO 120
   WRITE(6,1000)
1000 FFORMAT(10) EXECUTION TERMINATED. INPUT FCM OUTSIDE LIMITS 0 TO
   1220 DB.
   GC TO 9000
120 IF((NPLPTS-GE.0).AND.(NPLPTS.LE.250)) GO TO 130
1010 WRITE(6,1010) EXECUTION TERMINATED. INPUT NUMBER OF PROPLLOSS PTS
   15 OUTSIDE LIMITS 0 TO 250.
   GC TO 9000
C
C
C
130 READ(5,830) (IDATA(I),I=1,40)
830 FFORMAT(20A4)
C
C
C
140 READ THE PROPAGATION-LOSS CURVE IN 1 KYD INCREMENTS.
   READ(5,840) (PLOSS(I),I=1,NPLPTS)
840 FFORMAT(10X,10F7.1)
   CALL RANGE
   IF(INDEX,LT.11) GO TO 140
1020 FFORMAT(10,1020) EXECUTION TERMINATED. INPUT FCM IS TOO LOW TO PRODUCE
   15 DETECTIONS AGAINST THE INPUT PROPLLOSS CURVE.
   GC TO 9000
140 CALL GECH
   CALL TOSS
   CALL MEET
   CALL BUILD
   CALL MAKEUP
   CALL OUTPUT
9000 STOP
END

```

CARD00094
 CARD00095
 CARD00096
 CARD00097
 CARD00098
 CARD00099
 CARD0100
 CARD0101
 CARD0102
 CARD0103
 CARD0104
 CARD0105
 CARD0106
 CARD0107
 CARD0108
 CARD0109
 CARD0110
 CARD0111
 CARD0112
 CARD0113
 CARD0114
 CARD0115
 CARD0116
 CARD0117
 CARD0118
 CARD0119
 CARD0120
 CARD0121
 CARD0122
 CARD0123
 CARD0124
 CARD0125
 CARD0126
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 CARD0131
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 CARD0134
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 CARD0136
 CARD0137
 CARD0138
 CARD0139


```

100 INDEX = INDEX + 1
    IF (INDEX.EQ.11) GO TO 110
    IF (RANGES(INDEX).LE.(0.05*SUBSPD)) GO TO 100
110 RETURN
    END

```

```

CARD0188
CARD0189
CARD0190
CARD0191
CARD0192

```



```

110 IF(MODE.EQ.2) GO TO 110
    IBOYSP = 1.41421*ANGES(INDEX)
    IF( IBOYSP.LT.4) IBOYSP = 4
    BUOYSP = IBOYSP
    BMON = (BUOYSP/SUBSPD - 0.333333)/2.0
    IF(BMON.GT.1.0) BMON = 1.0
    IF(BMON.LT.0.166666) BMON = 0.166666
    IBOYSP = 60*BMON + 1
    UNMON(2) = BMON
    CYCLE(2) = 2.0*BMON
    UNMON(3) = CYCLE(2)
    CYCLE(3) = 3.0*BMON
    ERFRNG = RFRNG + 0.25*(BMON*ACSPD)
    NRBUCY = ((2*ERFRNG)/BUOYSP) + 1
    INSIDE = ((2*ERFRNG)/BUOYSP) + 1
    PCX = XP + SUBSPD*(TLATE + 1.0 + (6*ERFRNG)/ACSPD)
    BSUM = 0.0
    SHIFT = BUOYSP*(NRBUOY - 1)/2.0
    DO 120 I=1,NRBUOY
        PY(I) = BSUM - SHIFT
        BSUM = BSUM + BUOYSP
    CONTINUE
120 RETURN
    END

```

CARD0241
 CARD0242
 CARD0243
 CARD0244
 CARD0245
 CARD0246
 CARD0247
 CARD0248
 CARD0249
 CARD0250
 CARD0251
 CARD0252
 CARD0253
 CARD0254
 CARD0255
 CARD0256
 CARD0257
 CARD0258
 CARD0259
 CARD0260
 CARD0261
 CARD0262
 CARD0263
 CARD0264


```

SUBROUTINE TROSS
  DIMENSION RN(1500)
  COMMON MODE, BMON, ACSPD, SUBSPD, SUBCUS, CUSACC, IACSPD, IACALT, ISC
  1UBSP, ISUBCS, ICUSAC, FLATE, FCM, BUQYSP, IBOYSP, NPLPTS, INDEX, XI, CARD00266
  2YI, X2, Y2, DX, DY, RFRNG, NRBUOY, SHIFT, THETA, PCX, ICYCL, LINES, NSONO, PMAXX, CARD00267
  3, PLUS(250), RANGES(10), PY(150), DETECT(150), UNMCN(3), CYCLE(3), PD(3), CARD00268
  43), PVEC(3,48), IDATA(40) CARD00269
  DATA ISEED/8241905/ CARD00270
  CARD00271
  CARD00272
  CARD00273
  CARD00274
  CARD00275
  CARD00276
  CARD00277
  CARD00278
  CARD00279
  CARD00280
  CARD00281
  CARD00282
  CARD00283
  CARD00284
  CARD00285
  CARD00286
  CARD00287
  CARD00288
  CARD00289
  CARD00290
  CARD00291
  CARD00292
  CARD00293
  CARD00294
  CARD00295
  CARD00296
  CARD00297
  CARD00298
  CARD00299
  CARD00300
  CARD00301
  CARD00302
  CARD00303
  CARD00304
  CARD00305
  CARD00306
  CARD00307
  CARD00308
  CARD00309
  CARD00310
  CARD00311
  CARD00312

  MAKE NRTOSS RANDGM SIMULATIONS THROUGH THE SONOBUOY PATTERN AREA.
  HENCE, DETERMINE THE PROBABILITIES THAT A SUBMARINE WILL PASS
  THROUGH VARIOUS ZONES OF THE SONOBUOY PATTERN.

  NRTOSS = 500
  RNGSSQ = RANGES(INDEX)**2
  GAMMA = (1.5708 - SUBCUS) - THETA
  GSIN = SIN(GAMMA)
  GCOS = COS(GAMMA)
  CIRMALX = SHIFT + RANGES(INDEX)
  SQMXCR = CIRMALX**2
  MISS = 0
  DO 10 I=1, NRBUOY
    DETECT(I) = 0
    CCNTINUE
    NVEC = 3*NRTOSS
    CALL RANDOM(ISEED, RN, NVEC)
    DO 20 I=1, NRTOSS
      RX = DX*(2.0*RN(I) - 1) + I - 1
      RY = DY*(2.0*RN(I) - 1) + I - 1
      TEMPX = RX*GCOS - RY*GSIN
      TEMCUS = CUSACC*(2.0*RN(2*NRTOSS + I) - 1)
      TSIN = SIN(TEMCUS)
      TCOS = COS(TEMCUS)
      PHI = ATAN2(-TEMPY, (PCX - TEMPX))
      PSI = PHI - TEMCUS
      PCOS = COS(PSI)
      PSIN = SIN(PSI)
      IF(PSI.LT.0) PSI = -PSI
      SIDE1 = SQRT((PCX - TEMPX)**2 + TEMPY**2)
      IF(CIRMALX.SIDE1) GO TO 30
      SIDE2 = SIDE1*PSIN
      SIDE3 = SQRT(SQMXCR - SIDE2**2)
      DIST1 = SIDE1*PCOS + SIDE3
      INCP TO 40
    GO TO 40
  30 SIDE0 = SQRT(SIDE1**2 - SQMXCR)
    ALFA = ATAN(CIRMALX/SIDE6)

```



```

UP = PHI + ALFA
DCWN = PHICUS.GT.UP).OR.(TEMCUS.LT.DCWN)) GO TC 70
IF(SIDE2 = SQR(T(SQMXXCR - SIDE2**2)
INCR = SIDE3 + 1.0
SIDE4 = SIDE1*PCOS
SIDE5 = SIDE4 - SIDE5*TCOS
TEMPX = TEMPY + SIDE5*TSIN
TEMPY = TEMPY + SIDE5*TSIN
40 DC 50 J=1, INCR
DC 60 K=1, NRBUOY - PCX)**2 + (TEMPY - PY(K))**2
BUOYD = (GT.RNGSSQ) GO TC 60
IF(BUCYD.GT.RNGSSQ) GO TC 60
DETECT(K) = DETECT(K) + 1
GO TO 20
CCNTINUE
60 TEMPX = TEMPX + 2.0*TCOS
TEMPY = TEMPY + 2.0*TSIN
CCNTINUE
50 MISS = MISS + 1
70 CCNTINUE
20 CCNTINUE
90 CCNTINUE
DETECT(I) = DETECT(I) / NRTOSS
CCNTINUE
RETURN
END

```

CARD00313
 CARD00314
 CARD00315
 CARD00316
 CARD00317
 CARD00318
 CARD00319
 CARD00320
 CARD00321
 CARD00322
 CARD00323
 CARD00324
 CARD00325
 CARD00326
 CARD00327
 CARD00328
 CARD00329
 CARD00330
 CARD00331
 CARD00332
 CARD00333
 CARD00334
 CARD00335
 CARD00336
 CARD00337
 CARD00338
 CARD00339


```

SUBROUTINE MEET
COMMON MODE,BMON,IBMON,ACSPD,SUBSPD,SUBCUS,CUSACC,IACSPD,IACALT,IS
1UBSP,IUSPCS,ICUSAC,TLATE,FOM,BUDYSP,IBDYSP,NPLPTS,INSIDE,INDEX,XI,
2Y1,X2,Y2,DX,DY,REFRNG,NRBUOY,SHIFT,THETA,PCX,ICYCL,LINES,NSONG,PMAX
3,PLOSS(250),RANGES(10),PY(150),DETECT(150),UNMON(3),CYCLE(3),PD(3,
43),PVEC(3,48),IDATA(40)
CARD00340
CARD00341
CARD00342
CARD00343
CARD00344
CARD00345
CARD00346
CARD00347
CARD00348
CARD00349
CARD00350
CARD00351
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CARD00360
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CARD00362
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CARD00380
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CARD00385
CARD00386
CARD00387

FOR EACH COMBINATION OF SONOBUGY PATTERN ROWS AND PATTERN MONITOR
SEQUENCES BETWEEN 1 AND 3, THE PROBABILITY THAT A SUBMARINE WILL
BE DETECTED IN A ZONE UNDER THOSE CONDITIONS IS CALCULATED.
THESE ARE THE "MEETING" PROBABILITIES.

SPACE = BUDYSP
FILL1 = 0.05*SUBSPD
DO 10 I=1,3
IF(I.EQ.2) SPACE = SPACE/2.0
FILE2 = SPACE/2.0
DO 20 J=1,3
PSUM = 0.0
DO 30 K=1,10
RNGSSQ = RANGES(K)**2
IF(FILL1.LT.RANGES(K)) GO TO 40
PRCB = 0.0
GO TO 130
40 DIST2 = Sqrt(RNGSSQ - FILL1**2)
IF(J.GT.1) GO TO 50
IF(DIST2.LT.FILL2) GO TO 60
PRCB = 1.0
GO TO 130
60 PRCB = DIST2/FILL2
GO TO 130
50 FILL3 = UNMON(J)*(SUBSPD/2.0)
IF(FILL3.LT.RANGES(K)) GO TO 70
DIST1 = 0.0
GO TO 80
70 DIST1 = Sqrt(RNGSSQ - FILL3**2)
80 IF(DIST1.LT.FILL2) GO TO 90
PRCB = 1.0
GO TO 130
90 IF(DIST2.GE.FILL2) GO TO 100
DIST1 = DIST2 - DIST1
HT1 = FILL1
HT2 = FILL3
HTM1 = HT1 + HT2
DISTM2 = 0.0
HTM2 = 0.0
GO TO 120
100 IF((DIST1 + DIST2).LT.SPACE) GO TO 110

```

CC
CC
CC
CC
CC


```

DISTM1 = 0.0
HTM1 = 0.0
DISTM2 = 0.0
FILL2 = FILL2 - DIST1
HT1 = FILL1
HT2 = SQR1(RNGSSQ - FILL2**2)
HTM2 = HT1 + HT2
GO TO 120
110 DISTB = SPACE - DIST2
DISTM1 = DISTB - DIST1
FILL1 = FILL1
HT1 = SQR1(RNGSSQ - DISTB**2)
HTM1 = HT1 + HT2
DISTM2 = (DIST2 - DISTB)/2.0
HT1 = FILL3
HTM2 = HT1 + HT2
120 PART2 = 1.0 - ((0.1 + UNMON(J))**2 + (CYCLE(J) - HTM1/SUBSPD)**2)/
1((2.0*CYCLE(J)**2)
PART3 = 1.0 - ((0.1 + UNMON(J))**2 + (CYCLE(J) - HTM2/SUBSPD)**2)/
1((2.0*CYCLE(J)**2)
IF(I.NE.3) PROB = (DIST1 + DISTM1*PART2 + DISTM2*(PART3*(2 - PART3
1))/FILL2
IF(I.EQ.3) PROB = (DIST1 + DISTM1*(PART2*(3 - PART2))/2.0 + DISTM2
1*(PART3*(PART3 + 3)))/FILL2
130 PSUM = PSUM + PROB
30 PSUMINUE = PSUM/10.0
30 PD(I,J) =
20 CCNTINUE
10 CCNTINUE
END

```

CARD00388
 CARD00389
 CARD00390
 CARD00391
 CARD00392
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 CARD00399
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 CARD00415
 CARD00416
 CARD00417


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SLBROUTINE BUILD
COMMON MODE, BMON, IBMON, ACSPD, SUBSPD, SUBCUS, CUSACC, IACSPD, IACALT, ISC
1UBSP, 1SUBCS, ICUSAC, TLATE, FOM, BUOYSP, 1BOYSP, NPLPTS, INSIDE, INDEX, X1, CARD00419
2Y1, X2, Y2, DX, DY, RFRNG, NRBUOY, SHIFT, THETA, PCX, ICYCL, LINES, NSONC, PMAX, CARD00420
3, PLOSS(250), RANGES(10), PY(150), DETECT(150), UNMON(3), CYCLE(3), PD(3, CARD00421
43), PVEC(3,48), IDATA(40) CARD00422
CARD00423
CARD00424
CARD00425
CARD00426
CARD00427
CARD00428
CARD00429
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CARD00431
CARD00432
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CARD00458
CARD00459
CARD00460
CARD00461
CARD00462
CARD00463
CARD00464
CARD00465

THE ZONE PASSAGE PROBABILITIES (SUBROUTINE TOSS) ALONG WITH THE
ZONE MEETING PROBABILITIES (SUBROUTINE MEET) ARE PIECED TOGETHER TO
FORM PATTERN PROBABILITIES.

LOGICAL FLAG
LINES = 1
NSONC = 1
PMAX = 0.0
DO 10 I=1,3
  BUOY/2
  LSIDE = NRBUOY
  IF(LSIDE*2.NE.NRBUOY) LSIDE = LSIDE + 1
  FLAG = .FALSE.
  CYCL = 0.0
  ICYCL = 1
  DO 20 J=1, NRBUOY
    IF(I*J.GT.48) GO TO 10
    IF((J.GT.(INSIDE + 1)).OR.(I*J.GT.32)) GO TO 30
    IF(I*J.CYCL = ICYCL*2.EQ.J) GO TO 40
    OP = (J/2) + PD(I,K)*DETECT(LSIDE)
    IF(K.EQ.1) GO TO 50
    IF(OP = OP - PD(I,K - 1)*DETECT(LSIDE + 16/I) + PD(I,K)*DETECT(LSIDE
1+ 16/I) LSIDE - 1
50 LSIDE = LSIDE - 1
GO TO 60
40 OP = OP + PD(I,K)*DETECT(MSIDE)
GO TO 70
IF(K.EQ.1) GO TO 70
OP = OP - PD(I,K - 1)*DETECT(MSIDE - 16/I) + PD(I,K)*DETECT(MSIDE
1- 16/I)
70 MSIDE = MSIDE + 1
GO TO 60
30 IF(FLAG) GO TO 80
IF(FLAG = .TRUE.
  ICYCL = 3
  INNER = (16/I) - 1
  IF(INSIDE.LT.16/I) INNER = INSIDE - 1
  IF((J/2)*2.EQ.J) GO TO 90
  MIN = LSIDE
  MAX = MSIDE - 1

```


CARD00466
 CARD00467
 CARD00468
 CARD00469
 CARD00470
 CARD00471
 CARD00472
 CARD00473
 CARD00474
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 CARD00512
 CARD00513

```

    LSIDE = LSIDE - 1
    GO TO 100
  90  MAX = LSIDE + 1
    MSIDE = MSIDE + 1
    MID = MIN + (MAX - MIN)/2
  100  I1 = MID - INNER/2
    I2 = MIN + INNER
    I3 = MAX - INNER
    I4 = I1 + I2
    J1 = I3 - I4
    DO 110 N = MIN, J1
      CP = OP + PD(I, 3)*DETECT(N)
      CCNTINUE
  110  IF(I3 - I4) 120, 130, 140
  120  J1 = I3 - I4
    DO 150 N = I1, J1
      CP = OP + PD(I, 2)*DETECT(N)
      CCNTINUE
  150  DO 160 N = I3, I2
    CP = CP + PD(I, 1)*DETECT(N)
    CCNTINUE
  160  J1 = I2
    DO 170 N = J1, I4
      CP = OP + PD(I, 2)*DETECT(N)
      CCNTINUE
  170  GO TO 180
  130  DO 190 N = I1, I4
    CP = OP + PD(I, 2)*DETECT(N)
    CCNTINUE
  190  GO TO 180
  140  DO 200 N = I1, I2
    CP = OP + PD(I, 2)*DETECT(N)
    CCNTINUE
  200  J1 = I2 + 1
    DO 210 N = J1, J2
      CP = OP + PD(I, 3)*DETECT(N)
      CCNTINUE
  210  GO TO 220
  220  DO 220 N = I3, I4
    CP = OP + PD(I, 2)*DETECT(N)
    CCNTINUE
  230  J1 = I4 + 1
    DO 230 N = J1, MAX
      CP = OP + PD(I, 3)*DETECT(N)
      CCNTINUE
    GO TO 60

```



```

80 K = 1
   IF(I3.GE.I2) K = 2
   IF((J/2)*2.EQ.J) GO TO 240
   OP = OP + PD(I,3)*DETECT(LSIDE) - PD(I,K)*DETECT(I2) + PD(I,K + 1)
   1*DETECT(I2)
   LSIDE = LSIDE - 1
   I2 = I2 - 1
   GO TO 60
240 OP = OP + PD(I,3)*DETECT(MSIDE) - PD(I,K)*DETECT(I3) + PD(I,K + 1)
   1*DETECT(I3)
   MSIDE = MSIDE + 1
   I3 = I3 + 1
   60 IF((OP - PMAX).LT.0.00005) GO TO 250
   PMAX = OP
   LINES = LINES + 1
   NSONO = J*I = OP
250 PVEC(I,J) = OP
   20 CONTINUE
   10 RETURN
   END

```

CARD00514
 CARD00515
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```

SUBROUTINE MAKEUP
COMMON MODE,BMON,ACSPC,SUBSPD,SUBCUS,CUSACC,IACSPD,IACALT,IASCARD0535
1UBSP,I SUBCS,ICUSAC,TLATE,FQM,BUQYSP,IBOYSP,NPLPTS,INSIDE,INDEX,X1,CARD0536
2Y1,X2,Y2,DX,DY,RFRNG,NRBUOY,SHIFT,THETA,PCX,ICYCL,LINES,NSCNO,PMAX,CARD0537
3,PLDSS(250),RANGES(10),PY(150),DETECT(150),UNMON(3),CYCLE(3),PD(3,CARD0538
43),PVEC(3,48),IDATA(40)CARD0539
CARD0540
CARD0541
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CARD0560
CARD0561

C DATA SIGNIFICANT WHEN COMPUTING THE PROGRAM RESULTS IS OUTPUT.
C
C
900 WRITE(6,900)
FORMAT(1,59X,'NANCEE MAKEUP',/)
910 WRITE(6,910)
FORMAT(0,RANGES ARRAY',/)
920 WRITE(6,920) (RANGES(I),I=1,10)
FORMAT(,F10.1)
930 WRITE(6,930)
FORMAT(,///,DETECT ARRAY',/)
940 WRITE(6,940) (DETECT(I),I=1,NRBUOY)
FORMAT(,10F10.5)
950 WRITE(6,950)
FORMAT(,///,PD ARRAY',5X,'ROWS',5X,'SEQUENCES',/)
DC 10 I=1,3
WRITE(6,960) ((PD(I,J),I,J),J=1,3)
FORMAT(,F10.4,4X,12,9X,I2)
960 CONTINUE
10 RETURN
END

```



```

1010 IF(I.EQ.36) WRITE(6,1010) ISUBSP
    FORMAT(+,29X,'SUBMARINE SPEED:',13,' KNOTS')
1020 IF(I.EQ.37) WRITE(6,1020) ISUBCS
    FORMAT(+,29X,'SUBMARINE COURSE:',14,' DEGREES TRUE')
1030 IF(I.EQ.38) WRITE(6,1030) ICUSAC
    FORMAT(+,29X,'SUBMARINE COURSE ACCURACY:',14,' DEGREES EITHER SIDE OF COURSE')
1040 IF(I.EQ.39) WRITE(6,1040) X1,X2,X3,X4
    FORMAT(+,29X,'INITIAL SUBMARINE PROBABILITY AREA: X1=',F7.1,' X2=',F7.1,' X3=',F7.1,' X4=',F7.1)
1050 IF(I.EQ.40) WRITE(6,1050) Y1,Y2,Y3,Y4
    FORMAT(+,29X,'Y1=',F7.1,' Y2=',F7.1,' Y3=',F7.1,' Y4=',F7.1)
1060 IF(I.EQ.41) WRITE(6,1060) T,LATE
    FORMAT(+,29X,'TIME LATE:',F5.1,' HOURS')
1070 IF(I.EQ.42) WRITE(6,1070) IACSPD
    FORMAT(+,29X,'AIRCRAFT ON-STATION SPEED:',14,' KNOTS')
1080 IF(I.EQ.43) WRITE(6,1080) IACALT
    FORMAT(+,29X,'AIRCRAFT ON-STATION ALTITUDE:',16,' FEET',/)
1090 CONTINUE
    WRITE(6,1090) LINES,NSONG,PMAX
    FORMAT(+,14X,'OPTIMUM PATTERN:',12,' ROWS ',13,' SONOBUOYS -- PROBABILITY-OF-DETECTION=',F7.4)
1100 IF(NSROW.GT.44) GO TO 20
    DC 30 I=1,LINES
    J= (I-1)*NSROW + 1
    K = I*NSROW
    IF(NSROW.LE.21) WRITE(6,1100)
    FORMAT(+,7//)
    IF(NSROW.GT.21) WRITE(6,1110)
    FORMAT(+,7//)
    IF((I/2)*2.EQ.I) GO TO 40
    IF(NSROW.LE.21) WRITE(6,1120) (L,L=J,K)
    IF(NSROW.GT.21) WRITE(6,1130) (L,L=J,K)
    IF(NSROW.GT.44) GO TO 30
    GO TO 30
    IF(NSROW.LE.21) WRITE(6,1140) (L,L=J,K)
    IF(NSROW.GT.21) WRITE(6,1150) (L,L=J,K)
    IF(NSROW.GT.44) GO TO 30
    CONTINUE
    WRITE(6,1160)
    FORMAT(+,7//,' OPTIMUM PATTERN PARAMETERS',/)
1160 ICREN1 = ISUBCS + 90
    ICREN1 = ICREN1 - 180
    ICREN1 = ICREN1 + 180
    ICREN1 = ICREN1 + 180

```



```

IUREN2 = IUREN1 + 180
WRITE(6,1170) IUREN1, IUREN2
FORMAT(1,170) ORIENTATION: ',14,','/,13, ' DEGREES TRUE')
1170 WRITE(6,1180) IBOYSP
1180 WRITE(6,1180) SONOBUOY SPACING: ',14, ' NAUTICAL MILES')
1190 WRITE(6,1190) PCX, ISUBCS
1190 WRITE(6,1190) RANGE/BEARING FROM INITIAL SUBMARINE PROBABILITY AREA CCARD0664
1200 ENTER TO SONOBUOY PATTERN CENTER: ',F7.1, ' NAUTICAL MILES/,13, ' DECCARD0665
29 DEGREES TRUE')
IF (INSONO.GT.16) GO TO 60
WRITE(6,1200) MONITOR ALL PATTERN SONOBUOYS CONTINUOUSLY')
1200 GO TO 70
60 WRITE(6,1210) ICYCL, IBMON
1210 FORMAT(1,1210) USE: ',12,13, ' MINUTE MONITOR CYCLES')
70 WRITE(6,1220)
1220 FORMAT(1,1220)
RETURN
END

```

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CARD0676

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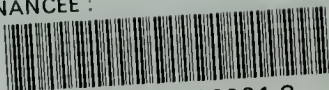
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